Thompson-Leroy
HOLTON TP.

121

LEVEL BOOK
373

KEUFFEL & ESSER CO.

DRAWING MATERIALS
AND
SURVEYING INSTRUMENTS.
NEW YORK.

CHICAGO. ST. LOUIS. SAN FRANCISCO. MONTREAL.

TABLES FOR EXCAVATIONS AND EMBANKMENTS.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.
ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.
FOR SINGLE TRACK RAILROADS.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	[illegible]	[illegible]	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	[illegible]	[illegible]	[illegible]	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	[illegible]	[illegible]	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	[illegible]	[illegible]	[illegible]	12.5	[illegible]	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

Thompson - Leroy Rd. CH. 7
Levels first culvt E of
Cemetery. Pg 74-75

X-Sections pg. 4-30
Slope Stakes pg. 31-51
Grade Stakes pg. 52-73

Thompson Rd CH 7 Sec. E.
Profile Levels Pg. 77

Thompson Rd Sec "C" Pg. 70
Culvt. Levels Sta.

(21)

B. M.'s

B.M. #1. Spike in N. Root 14" Maple
33' Rt. Sta 0+10
Elev. 1069.97

B.M. #2 Spike in S.W. Root 16" Maple
31' Rt Sta 5+05
El. 1075.18

B.M. #3 Spike in So. Root 16" Maple
27' Lt. Sta 10+55
El. 1076.92

B.M. #4. Bent Spike in N.W. Root
16" Maple 28' Rt. Sta 17+50
El. 1074.25

B.M. #5 Spike in E. Side C.E.I. Pole #289452 21' Lt. Sta 24+30 El. 1073.25

B.M. #6 Spike in E. Root 24" Maple 23' Lt. Sta 30+64 Elev. 1080.47

B.M. #7 Spike in N. Root 18" Maple 32' Rt. Sta 37+34 Elev. 1085.61

B.M. #8 Bent Spike in E. Root 12" Maple 28' Lt. Sta 43+55 Elev. 1092.43

B.M. #9 Spike in N. Root 24" Elm 27' Rt. Sta 47+95 Elev. 1096.45

B.M. #10 Spike in So. Root 15" Pine 41' Lt. Sta 59+51 Elev. 1107.44

B.M. #11 Spike in So. Root 14" Maple 32' Lt. Sta 67+90 Elev. 1111.70

B.M. #12 Spike in No. Root 14" Maple 27' Rt. Sta 74+68 Elev. 1122.95

B.M. #13 Spike in N.W. Root 14" Maple 34' Rt. Sta 79+48 Elev. 1130.00

B.M. #14 Spike in No. Root 14" Maple 36' Rt. Sta 85+51 Elev. 1141.08

B.M. #15 2 Spikes in C.E.I. Pole
#73438 25' Rt. Sta 90+69
Elev. 1160.10

B.M. #16 X on N.W. Corner So. Hd Wall
Side Rd. Culvert Sta 98+53
El. 1188.49

B.M. #17 Spike in S.E. Side 10" Maple
25' Lt. Sta 112+47
Elev. 1205.66

B.M. #18 Spike in N. Side 10" Catalpa
27' Lt. Sta 117+74
El. 1217.67

B.M. #19 Spike in So. Root
40" Chestnut 34' Lt.
Sta 123+44
Elev. 1252.64

B.M. #20 Spike in N.W. Root
14" Maple 29' Rt.
Sta 129+47
Elev. 1249.56

B.M. #21 Spike in S.W. Root
14" Maple 30' Lt.
Sta 141+14
Elev. 1260.73

B.M. #22 Spike in S.W. Root 20" Maple
31' Rt. Sta 150+84
Elev. 1271.80

U.S.G.S. B.M. Bronze Tablet in
S.W. Corner Stone
Found. Congreg. Church
Stamped "1277" Cleveland
Elev. 1276.266

This Tablet
td June 1957
Bldg is now
P. Robinson Garage
Located 16.1' from SWt on front Wall

Thompson - Leroy Rd

Sta	+	H.I.	-	Elev.	Rem's.
B.M.	2.15	1072.12		1069.97	Spike in N. Root of 14" Maple 33' Rt Sta 0+10 El. 1069.97
-1+0	℄ 8'x4' Conc Culvert				Outlet channel to be Cleaned
0+00.4	End of Pavement (10' Conc)				
0+39	℄ Drive South				
+65					
1+0					
1+50					
2+0					
T.P.	5.54	1075.53	2.13	1069.99	
+12.2	℄ 3'x3'x20 Conc. Box Culvert				
3+0					

Oct. 14, 1930 (Fair)

S. Gold Jr.
S. Merritt
H. Barton

4

South ℄ North

9.7/50' 10.9/F.L.+3.0/14.0 5.54 5.55 6.38/14.0 6.78 6.39/13.5 5.55 5.5 11.2/F.L. 11.0/25' 11.6/75'

3.3/30 3.6/26 6.7/16 6.1/15 5.9/13 5.5/10 4.83/25 Edge Pave. 4.85 5.10/8' N Edge Pave. 5.3/11 6.7/15 6.5/17 5.6/19 5.9/22 7.1/30

+0.5/H 2.4/30 3.9/12 4.2/9 4.0

1.2/30 1.4/22 4.6/15 4.6/14 4.2/12 3.9/9 3.3 3.9/5 4.4/9 4.9/12 5.0/15 2.6/19 2.4/22 2.6/30

1.1/30 1.5/27 4.3/17 4.3/14 3.6/13 3.9/11 3.3/7 3.2 3.9/7 4.5/11 4.4/13 2.3/17 2.3/22 2.5/30

1.7/30 1.8/28 1.8/22 3.9/16 4.6/14 3.8/12 3.8/11 3.4/2 3.6 4.2/7 4.3/8 4.9/10 5.0/14 3.8/16 3.8/19 4.0/22 6.7/30

6.2/30 5.9/25 6.2/19 6.7/17 3.4/10 3.4/9 3.9/3 3.3 3.5/4 6.3/10 6.8/16 7.0/23 7.5/30

10.8/50 11.0/30 11.5/F.L.+2.7 5.4 5.5/11.2 6.2/11.2 6.6/9 6.1/2 6.3 6.5/4 6.2/5.8' 5.8/5.8' 5.8/7.3' 11.3/F.L. 12.1/25' 12.9/100' 15.0/175'

10.7/150 10.5/175' 10.7/100' 11.0/75'

6.5/19 7.7/17 7.7/15 7.0/14 6.5/12 5.9/4 6.1 6.5/5 6.7/7 7.4/10 8.2/13 7.3/15 4.6/22 3.8/27 3.9/30

6.6/24

6.6/30

Sta	+	H.I.	−	Elev	Remarks
		1075.52			
4+00				1075.18	Rec.
B.M. & T.P.	3.86	1079.04	0.36	1075.17	Spike in S-W Root 16" Maple 31' ℄ Sta 5+05 El. 1075.18
+30	℄	Drive	South		
+42	℄	Culvert (			
5+00					
6+00					
7+00					
8+00					
T.P.	5.40	1080.48	3.96	1075.08	
9+00					
10+00					
B.M.			3.56	1076.92	Rec. 1076.92 Spike in S. Root 16" Maple 27' Lt. Sta 10+55

South ℄ North

2.0/30 2.3/26 2.9/19 3.3/18 3.3/16 3.0/15 3.1/14 2.6/5 2.9 3.3/4 3.2/5 3.7/8 4.3/11 4.3/13 2.9/15 2.4/17 2.0/23 2.0/30

1.2/FL

3.4/FL 5.0/30 5.5/13 5.2/5 6.5

5.2/30 5.4/23 6.8/20 6.9/FL→18 4.9/15 5.2/4 4.7/6 5.0 5.2/3 5.2/5 5.4/8 7.2/FL 7.2/14 5.7/16 4.8/21 4.8/25 5.3/30

4.5/30 5.2/21 5.6/19 6.5/18 6.3/15 5.9/13 4.8/1 4.9 5.2/6 5.4/9 5.4/11 6.1/13 6.1/14 4.8/16 4.4/21 5.0/30

3.6/30 4.3/22 5.0/17 5.8/16 5.7/15 5.2/14 4.7/9 4.6 5.1/10 5.4/14 4.3/16 3.8/25 4.3/30

3.8/30 4.0/25 4.7/17 5.4/16 4.8/14 4.3/9 4.0 4.8/10 5.3/14 4.2/15 4.1/22 4.0/30

3.4/30 3.6/25 4.4/17 5.2/16 4.7/14 4.4/11 4.1 4.5/11 5.0/13 4.2/16 3.8/25 3.7/30

4.7/30 4.7/25 5.1/16 6.4/15 5.9/13 5.3 5.3/2 5.8/12 6.1/15 5.3/16 5.3/22 4.8/26 5.2/30

4.3/30 4.9/17 5.9/15 5.7/14 5.2/13 4.7/3 4.7 5.0/7 5.3/12 5.8/14 4.7/16 4.6/26 4.7/30

Sta	+	H.I	−	Elev.	Remks
		1080.48			
11+0					
12+0					
T.P.	4.46	1085.71	4.23	1076.25	
13+0					
14+0					
15+0					
16+0					
+45	℄	Drive (Both Sides)			
17+0					
B.M. & T.P.	2.09	1076.34	6.46	1074.25	1074.25 Rec.
18+0					Dent Spike in N.W. Root 12" Maple 28' Lt Sta 17+50 El. 1074.25

South ℄ North

					4.2	4.9 / 11	4.9 / 13	5.4 / 15	4.4 / 16	4.4 / 25	4.5 / 30
4.1 / 30	4.6 / 17	5.6 / 12	4.9 / 13	4.8 / 10	4.2	4.9 / 10	5.3 / 14	5.6 / 15	4.4 / 12	4.6 / 25	4.7 / 30
4.2 / 30	4.7 / 26	5.0 / 17	6.1 / 15	5.4 / 13	5.4 / 10	4.7	5.4 / 10	5.7 / 14	6.1 / 15	5.0 / 17	4.9 / 28	4.9 / 30
4.7 / 30	4.8 / 24	5.3 / 16	6.3 / 15	5.7 / 13	5.6 / 10	4.8	5.1 / 5	5.6 / 7	5.5 / 12	5.6 / 13	6.4 / 15	5.2 / 17	5.1 / 30
4.5 / 30	4.6 / 22	5.2 / 16	6.3 / 14	5.5 / 13	4.8	5.5 / 10	5.4 / 11	5.8 / 14	6.6 / 15	5.4 / 17	5.1 / 27	4.8 / 30
4.5 / 30	4.6 / 27	4.7 / 21	5.1 / 17	6.5 / 14	5.9 / 12	5.2	5.9 / 13	6.7 / 15	5.5 / 17	5.1 / 27	5.2 / 30
5.2 / 30	5.9 / 16	6.9 / FL 14' Plank Dr.	6.2 / 12	6.3 / 9	6.6 / 8	6.2	6.2 / 14	7.0 / 17	5.6 / 30 FL. Plank Dr.			
(4.8 / H)	5.5 / 30	5.6 / 21	6.0 / 15	8.3 / 13	8.1 / 10	7.8	8.2 / 12	8.7 / 15	7.1 / 17	6.4 / 26	6.3 / 30		
6.5 / 30	6.7 / 23	5.9 / 18	5.8 / 15	6.4 / 14	6.3 / 13	5.8 / 12	5.4 / 9	4.8	4.8 / 2	5.5 / 10	5.8 / 13	6.2 / 14	6.3 / 15	5.6 / 17	5.1 / 23
														6.2 / 30	

Sta	+	H I	-	Elev.	Remarks
		1076.34			
18+66	℄	3'x2' Culvert (Stone)			
19+0					
20+0					
T.P.	3.12	1077.49	1.97	1074.37	
20+47					
21+0					
22+0					
+68	℄	Drive North			
23+0					
+25	℄	2½x2½ Stone Culvert			

South ℄ North

7.9/19' 8.5/FL→13.8' 4.5/12 4.5/12 5.1/12 4.5/1 4.6 5.1/8.2 4.5/8.2 4.6/9.7 8.7/FL. 8.6/30 9.0/60 7.6/90 7.8/60 8.1/40 8.8/90' 9.8/120' 10.3/150'

3.7/23 4.6/17 6.1/16 6.1/15 5.0/13 4.9/11 4.4/3 4.4 4.9/10 4.7/12 5.3/14 4.0/12 3.6/24 3.5/30 3.2/30

1.1/30 0.9/20 1.4/17 2.5/15 2.5/14 2.1/13 1.9 1.9/4 2.3/13 2.7/14 1.9/16 1.6/21 1.7/30

1.9/30 1.9/21 2.0/16 3.2/15 3.2/14 2.9/12 2.7 2.8/4 3.1/13 3.6/14 3.6/15 3.0/16 3.0/27 3.1/30

2.2/30 2.1/25 2.2/18 3.6/16 3.6/15 3.5/14 3.2 3.2/4 3.5/12 4.1/14 3.1/16 3.1/21 3.0/30

4.3/30 4.5/25 4.9/18 6.0/16 6.0/14 5.7/12 5.4/5 5.2 5.4/4 5.7/10 5.9/12 6.3/14 5.8/16 5.1/19 5.2/30

6.0 6.1/9 6.1/14 7.4/FL. Pipe 6.2/30 (3.4/H)

6.8/30 6.8/24 7.0/19 7.7/18 7.7/16 6.2/12 5.8/4 5.8 6.2/9 7.8/12 7.9/14 7.1/15 7.2/21 7.6/30

7.6/30 8.2/34 9.0/17' 9.5/FL→9.3 4.3/7.5 4.4/7.5 5.3/7.6' 5.4 5.8/11.3 6.3/13.3 9.9/FL. 9.8/27' 10.4/80' 10.7/100'

6.9/15' from ℄ 7.3/80

Ld Ditch (Hell's Hollow)

11.8 Ld

Inlet Plank Bridge (9'x4') Hell's Hollow

Sta	+	H.I	-	Elev	Rem's	South	℄	North
		1077.49						
23+68.38 P.C.				1073.25 Rec.		6.4/23 6.7/20 7.4/19 7.5/17 6.9/15 6.2/12 6.1/5 5.3/30 5.7/25	5.8	5.9/5 6.6/16 7.3/27 7.7/40
B.M.	5.88	1079.14	4.23	1073.26	Spike in E Side C.E.I. Pole #289452 21' Lt. PC.+62 (Sta 24+30±) El. 1073.25			
24+0						6.1/28 6.5/24 7.9/19 8.7/17 8.6/15 7.9/14 8.0/11 6.1/30	7.4	7.9/11 8.6/24 8.9/35
+09± ℄ Hell's Hollow Rd.							7.4	7.9/7 7.9/35 9.4/60 9.7/120' 9.4/ ℄ Top Plank Bridge 175'±
+25						4.6/25 4.9/22 6.6/17 8.3/16 8.4/15 7.7/13 7.2/3 4.3/30	7.2	7.6/7 8.6/19 9.0/20' 8.0/21' 7.2/33'
+42 ℄ Drive North							7.0	7.4/10 7.5/17 8.4/F.L. Tile 6.7/30 (4.0/H.)
+50						3.8/27 4.0/24 4.3/18 5.5/15 7.5/14 7.5/12 7.1/11 7.2/10 3.4/30	6.7	7.1/13 8.3/14 7.0/17 6.5/30
+75						2.6/27 3.1/23 3.5/18 4.0/15 7.1/13 7.1/12 6.6/11 2.9/30	5.9	6.4/8 6.8/12 7.1/13 5.4/16 5.0/23 4.8/30
25+0						2.5/24 2.8/23 2.9/17 3.6/15 6.2/12 6.2/11 6.1/9 2.8/30 2.6/28	5.4	5.7/9 6.2/13 4.5/15 4.6/24 4.3/30
+25						2.9/30 2.4/27 2.9/19 3.5/15 5.9/13 5.7/10 5.4/6	5.0	5.0/5 5.4/10 5.8/13 3.9/15 4.0/23 3.9/30

Sta	+	H.I	-	Elev.	Rem's
		1079.14			
25+50					
+65.31	P.T.				
26+0					
T.P.	6.50	1082.46	3.18	1075.96	
+64	Drive North				
27+0					
28+0					
29+0					
30+0				1080.47	
B.M. & T.P.	4.40	1084.87	2.00	1080.46	Spike in E. Root 24" Maple 23' Lt Sta 30+64 El. 1080.47
31+0					

South	℄	North
3.0/24 3.0/19 3.5/17 5.3/15 5.4/13 5.2/12 4.9/7 ; 2.3/30 2.3/28	4.6	4.6/4 4.9/12 5.4/13 4.2/15 3.9/17 3.8/27 4.2/30
3.2/19 3.5/17 5.2/15 5.2/14 4.9/13 4.6/6 ; 3.2/30 2.5/27 2.8/24	4.3	4.3/6 4.6/12 5.1/15 3.8/16 3.7/26 3.8/30
2.1/27 2.6/22 3.2/17 4.8/16 4.9/15 4.5/14 4.0/6 ; 2.6/30	3.7	3.8/5 4.1/11 4.8/15 3.6/17 3.5/24 3.4/26 3.8/30
	6.2	6.6/15 7.1 (← FL, → Pipe) 6.3/19 6.2/30
4.6/30 5.1/25 5.5/18 7.1/16 7.2/14 6.6/13 6.4/10	5.8	5.9/3 6.3/11 6.2/13 6.8/15 6.8/16 6.0/17 5.9/24 6.0/30
5.4/17 6.4/16 6.4/15 5.8/13 5.5/12 5.5/10 5.1/4 ; 5.5/30 5.0/24	4.9	4.9/3 5.5/9 5.7/12 5.4/13 6.2/14 6.4/16 5.7/17 5.6/23 ; 5.5/26 5.8/30
3.9/30 3.8/22 4.4/17 5.7/15 5.8/14 5.3/13 5.0/10 4.5/3	4.3	4.4/3 4.7/8 5.1/13 5.8/15 5.9/16 5.2/17 4.9/21 4.6/27 ; 4.5/30
3.7/30 3.8/26 4.1/16 4.9/14 4.8/13 4.3/12 4.2/8	3.6	3.7/4 4.0/11 4.2/13 4.7/15 4.8/16 4.1/17 4.0/22 3.7/27 3.9/30
5.1/30 5.1/18 5.5/15 6.4/14 6.5/13 5.9/12 5.8/8 5.5/4	5.1	5.2/4 5.8/13 6.4/15 6.6/16 5.9/17 5.8/20 5.7/25 5.6/30

OCT. 15' 1930 (Fair)

Sta	+	H.I.	−	Elev.	Rem's
		1084.87			
32+00					
T.P.	4.57	1086.95	2.49	1082.38	
33+00					
+53.60	P.C.				
+75					
34+00					
+25					
+50	Also	Drive	North		
+80.98	P.T.				
35+00					
T.P.	5.42	1087.21	3.16	1083.79	

S Gold dr.
S Merritt
H Barton

10

South ℄ North

3.7/30	3.9/23	3.4/17	3.9/14	6.3/13	4.6/11	4.8/9	4.2	4.2/4	4.8/13	5.2/15	5.2/16	4.6/17	4.4/21	4.3/25	4.9/30
3.8/30	4.2/18	4.6/14	5.9/13	5.8/12	5.4/10	5.5/8	5.0	5.0/4	5.8/13	6.1/14	4.9/16	4.8/24	4.7/30		
2.9/30	3.1/23	3.5/15	4.7/13	4.5/12	4.5/11	4.7/10	4.6/5	4.7	4.7/4	5.0/11	4.8/12	5.0/13	5.1/14	4.0/16	3.8/25	3.8/30
2.2/25	2.1/21	3.0/15	3.8/14	4.8/13	4.1/12	4.1/10	4.4/9	4.2	4.4/10	4.1/11	4.2/13	4.4/14	3.3/16	3.3/25	3.4/30	
		2.15/30														2.4/H
1.5/30	2.0/21	2.6/16	3.7/13	3.6/10	3.8/9	3.9	3.9/4	4.1/10	3.9/11	4.0/13	3.8/14	3.2/16	2.9/24	2.9/30		
2.5/30	2.8/22	3.1/18	3.7/15	3.7/13	3.7/9	3.6	3.7/10	3.4/14	3.1/17	2.9/21	2.9/30					
2.4/30	2.6/23	3.1/16	4.0/15	3.5/13	3.5/9	3.3	3.3/3	3.4/10	3.3/14	2.9/18	2.8/23	3.1/26	3.2/30			
2.4/30	2.7/23	3.1/16	3.9/14	3.4/11	3.2	3.4/11	3.6/13	3.0/15	2.6/19	3.0/30						
2.3/30	2.7/23	3.7/15	4.1/13	3.5/11	3.6/9	3.5	3.5/9	3.8/13	4.0/15	3.5/16	3.0/23	2.8/25	2.7/30			

Sta	+	H.I.	−	Elev.	Rem's
		1089.21			
35+84	℄	3'x11/2' Stone Culvert			
36+0					
37+0				1085.61	
B.M. & T.P.	7.13	1092.74	3.60	1085.61	Spike in N. Root 18" Maple 32' Rt Sta 37+34 El. 1085.61
38+0					
39+0					
+24	Ditch Running South				
40+0					
+27	(West Ditch Road Running North)				
+39.5	℄ Road Running North				

11

South ℄ North

6.6/100' 7.4/50' 7.5/30' 8.1 FL.+8.1 4.2/6.6 5.4/6.6 5.1 5.3/9.4 4.3/9.4 4.2/10.9 8.1 FL. 8.0/25' 8.6/50 9.6/85 10.2/100'

4.9/30 2.5/23 4.1/18 5.9/15 7.2/14 7.3/11 5.5/9 5.2/7 5.3/6 4.9 5.3/8 5.1/9 5.9/12 7.4/14 7.2/15 6.0/17 6.3/23 6.4/27 6.5/30

6.0/30 5.1/23 5.0/19 5.4/15 6.7/13 6.4/12 5.8/11 5.3/9 5.4/8 4.8 4.8/1 5.4/10 5.2/11 6.7/13 6.4/15 5.3/16 5.2/21 4.7/27 4.7/30

6.5/30 6.4/24 6.6/18 8.3/16 8.4/12 7.3/10 7.1/8 6.9 6.5/1 7.8/10 7.9/11 8.6/12 9.3/14 9.2/15 7.8/16 6.7/23 6.2/26 5.9/30

4.7/19 6.1/17 7.0/16 7.7/14 7.7/13 7.2/12 5.7/11 5.6/10 5.4 5.9/9 6.2/11 7.5/13 7.7/15 7.2/16 6.3/18 5.6/19 5.1/24 4.5/30 4.7/25 4.7/30

5.6/35' 6.5/17' 7.4/14'

3.7/30 3.9/25 3.9/18 3.9/16 5.9/13 5.0/11 4.2/10 4.3/9 4.1 4.5/10 5.7/13 6.0/15 6.4/16 5.8/17 4.7/19 4.3/20 3.7/24 3.6/30

(4.1/H)

3.8 3.8/11 4.7/15 5.0/17 5.7/19 FL Pipe 5.5/20 5.3/34 4.9/100'

3.5 3.6/18' 3.1/100'

Sta	+	H.I.	−	Elev.	Rem's
		1092.74			
40+74	E. Ditch	Rd Running	North)		
41+0					
42+0					
T.P.	6.10	1096.43	2.41	1090 33	
+78	℄	Dr. North		1092.43	
B.M.			4.01	1092.42	Spike in E root 12" Maple 28'L 347 43+55 El. 1092.43
43+0					
44+0					
45+0					
46+0					
47+0					
T.P.	7.97	1101.34	3.06	1093.37	

South ℄ North

3.0 3.2/12 4.9/11 → F.I. Pipe 4.7/40' 4.5/100'

2.7 2.7/30 2.8/24 2.8/18 4.6/15 4.8/11 3.3/9 2.7 3.1/9 3.1/10 4.1/12 4.7/13 4.7/14 4.2/15 3.3/18 3.3/20 3.4/26 3.4/30

2.1/30 2.1/25 2.3/20 3.1/16 4.4/15 4.5/13 4.0/12 3.7/10 3.4/9 2.7 2.8/6 3.1/12 3.9/13 4.2/14 4.1/15 3.4/16 2.7/18 2.2/21 2.6/22 2.3/25 2.4/30

5.7 5.8/4 6.4/11 7.3/14 6.2/16 5.5/24 5.4/30

5.1/30 5.0/22 5.6/17 7.4/15 7.6/14 7.0/13 6.5/10 5.7 6.0/60 6.4/12 7.1/14 6.8/15 5.7/17 5.5/23 5.1/27 4.7/30

4.2/25 4.5/20 5.2/17 6.0/16 7.0/15 7.0/14 6.5/12 6.0/10 5.2 5.2/3 6.0/13 6.3/14 4.6/16 4.3/25 4.3/30 4.3/30

3.6/30 3.6/21 4.1/18 4.7/16 6.3/15 6.2/13 5.5/10 5.1/7 4.6 4.5/4 5.2/13 5.4/14 3.5/17 3.4/25 3.4/30

2.7/25 3.3/20 4.0/16 5.4/14 5.4/12 4.8/11 4.4/7 4.0 4.0/6 4.5/13 4.5/15 3.1/16 3.0/23 2.7/27 2.7/30 2.8/30

2.6/30 2.5/24 2.7/18 3.7/16 4.6/15 4.6/14 4.0/13 3.3/9 2.7 2.7/3 3.3/9 3.8/13 2.1/12 2.1/24 2.2/30

Sta	+	H.I.	−	Elev.	Remarks
		1101.34			
48+0				1096.45	
B.M.			4.91	1096.43	Spike in N Root 24' Elm 27' Rt Sta 47+95 El. 1096.45
49+0					
50+0					
51+0					
T.P.	8.00	1106.83	2.51	1098.83	
52+0					
53+0					
54+0					
55+0					
T.P.	4.05	1108.85	2.03	1104.80	
56+0					

South ℄ North

57/30 57/24 6.3/17 6.8/16 8.3/13 7.1/10 6.4 6.5/3 2.6/14 6.4/17 6.2/22 5.9/28 6.0/30

4.4/30 4.3/25 4.6/20 5.3/17 7.0/14 6.7/13 5.7/9 5.3/4 5.1 5.2/3 6.0/12 4.4/13 4.6/15 4.6/19 4.7/24 4.8/30

2.9/24 3.7/18 4.5/16 5.5/15 5.4/13 5.1/11 4.8/9 4.2/3 4.1 4.1/2 4.7/13 5.3/14 3.9/16 3.7/23 3.8/30 2.7/30

1.5/30 1.4/24 1.5/21 2.1/17 4.2/14 4.7/13 3.7/12 3.6/11 2.8 2.8/2 3.6/13 3.9/14 2.3/16 2.2/22 1.8/25 1.6/30

5.1/27 5.4/23 5.8/17 6.2/16 8.4/14 8.4/13 8.1/12 7.8/10 7.2/2 7.1 7.3/4 7.7/12 7.9/13 5.9/15 5.5/17 5.3/24 5.4/30 5.9/30

4.4/30 4.8/25 5.1/18 5.5/16 7.2/15 7.1/14 6.4/13 5.9/10 5.6/6 5.4 5.4/2 5.8/8 6.3/12 6.8/13 5.5/15 5.4/22 5.5/30

3.3/30 3.4/23 3.9/16 5.9/15 5.2/13 4.6/12 4.2/6 4.1 4.3/4 4.6/9 5.1/12 5.6/13 3.8/15 3.6/22 3.9/30

2.1/30 2.3/24 2.5/19 3.8/16 4.9/15 4.8/14 4.2/13 3.8/11 3.4/4 3.4 3.5/3 3.8/8 4.4/12 4.8/14 3.4/16 2.9/18 2.9/25 3.1/29 2.9/30

4.4/30 4.1/26 4.4/18 4.8/15 4.7/14 5.1/12 5.0/6 4.7 4.8/2 5.6/9 6.1/13 6.6/14 5.1/16 5.1/26 4.9/30

Sta	+	H.I	−	Elev.	Remarks
		1108.85			
57+0					
+ 68.7 ℄		9.1 × 2½' Culvert			
58+0					
59+0					
+ 15					
T.P.	8.30	1113.30	3.85	1105.00	
+ 78	℄	Drive	North		1107.11
B.M.		-	5.87	1107.43	
60+0					
61+0					
62+0					
T.P.	4.91	1115.85	2.36	1110.94	

South ℄ North

54/30 6.0/20 6.4/18 7.0/17 6.8/16 6.2/15 6.0/12 5.1/10 4.8/5 4.8 5.2/6 6.6/10 5.4/14 5.6/28 5.0/30

4.8/30 4.1/26

7.2/100 7.5/30 7.5/FL+11.3 2.9/11 2.9/11 4.2/11 3.9 4.1/7.3 2.9/7.3 2.9/8.2 ± FL 7.6/30 7.8/65 8.3/100 8.8

5.7/30 5.6/26 5.7/19 6.6/11 6.7/15 3.9/9 3.8 4.4/7 6.3/12 6.6/15 5.9/17 6.6/23 6.0/30

4.5/30 4.1/24 4.1/17 5.6/15 5.5/14 5.1/13 4.7/11 3.8/9 3.6 4.2/9 5.0/14 4.4/16 4.1/20 3.8/24 2.5/30

0.8/30 1.7/22 2.8/19 5.0/16 5.4/15 5.3/14 4.9/13 4.6/12 3.7/9 3.2 3.8/8 4.4/11 4.7/12 4.7/14 4.2/15 3.7/22 3.0/30

6.6 6.9/13 ± FL 7.7 Pipe 6.2/30 (5.4/H.I.)

3.8/30 4.1/24 3.9/17 6.5/15 7.4/14 7.4/11 6.9/9 6.2 6.4/3 6.9/10 7.2/12 7.6/13 7.4/14 5.6/17 5.7/24 5.3/30

3.2/30 3.5/24 3.7/17 5.5/15 5.7/14 5.4/12 4.6/9 4.3 4.3/4 4.9/12 5.1/14 5.2/15 4.5/17 4.3/22 4.1/30

2.1/30 2.8/23 3.0/16 4.5/14 4.6/13 4.3/12 3.7/8 3.7/7 3.3 3.3/3 3.4/12 4.3/13 4.3/15 3.7/16 3.5/W 3.9/30

Sta	+	H.I. 1115.85 −	Elev.	Rem's
63+00				
+25	℄	N & S. Road (Clay St)		
+36.56	P.C.			
+50				
64+00				
64+08	℄	Pipe Culvert (Hillside)		
+50				
65+00				
+50				

South ℄ North

49/30 51/22 5.2/9 5.3 5.4/3 5.9/9 6.2/13 6.9/15 6.9/16 7.1/18 6.7/20 5.6/24 6.6/30

42/100 47/75 5.1/14 5.3 5.9/8 6.7/25 8.0/100

5.2/30 5.0/14 5.2 5.9/8 6.5/19 6.6/24 6.8/30

5.4/30 5.1/15 5.0/5 5.1 5.4/4 5.1/6 5.8/12 6.7/25 7.0/30

4.8/30 5.3/27 5.4/22 5.9/18 6.4/17 6.2/14 5.3/14 5.1/6 5.4 5.9/5 7.6/9 7.8/12 8.1/13 7.8/14 7.3/16 6.1/18 5.8/22 6.9/30

4.6/30 5.1/20 7.0/FL 5.4/14.3 5.4 5.7/4 6.8/6 7.8/FL 8.0/11 5.4/18 5.8/30

4.9/30 5.1/21 6.0/19 6.6/18 5.7/16 5.2/6 5.5 5.8/3 6.4/5 5.5/10 5.1/12 5.4/18 5.5/26 6.4/30

4.3/23 5.1/21 4.9/20 5.8/18 6.5/17 6.3/16 5.9/15 5.7/14 5.5 6.0/5 6.3/7 5.5/8 5.1/10 5.0/16 5.5/25 5.9/30 4.3/30 4.6/25

5.3/19 5.5/17 6.1/16 6.8/15 6.7/14 6.7/13 6.0/12 6.1/11 5.6/2 5.7 5.8/3 6.1/7 6.0/9 7.2/11 6.3/12 6.4/14 5.8/17 5.9/23 6.3/30 4.5/30 4.9/25 5.0/22 4.7/21

Sta	+	H.I.	−	Elev	Rem's
		1115.85			
66+00					
+50					
+91	℄	culvert			outlet channel runs N. 100' then Nest to N 25 RR culvert
67+00					
+48.20	P.T.				
B.M.E.T.P.	5.29	1116.97	4.17	1111.70	1111.68
68+00					
+36	℄	Drive North			
69+00					
70+00					

South ℄ North

5.4/30 5.7/22 6.1/14 6.6/13 7.2/12 6.7/11 6.3/9 5.9 6.2/9 6.2/10 7.1/11 6.5/13 6.5/16 6.1/21 6.3/26 6.3/30

6.0/30 6.1/18 6.9/13 7.4/12 7.3/11 6.4/10 6.2/8 5.9 6.2/8 7.0/11 7.0/12 6.3/14 7.0/20 7.0/26 7.2/28 7.2/30

7.2/100' 8.8/F.L+10.2 4.3/8.7 4.3/8.7 5.1/8.7 5.0 5.1/10.3 4.3/10.2 4.3/11.8 8.8/F.L 8.9/30' 8.6/100' 9.9/200' 11.3/300' 13.5/400'

6.3/30 6.3/21 6.3/16 7.0/14 7.8/13 6.1/11 5.3/8 5.3/7 5.2 5.4/8 6.5/10 7.0/13 7.4/14 6.9/15 6.3/17 6.7/30

5.9/30 6.1/24 6.2/17 6.0/15 5.8/11 6.6/9 5.8/7 5.6 6.5/2 6.8/11 6.5/13 6.9/14 6.3/15 6.2/19 6.1/28 6.2/30

6.3/30 6.7/21 6.7/16 6.8/10 7.4/9 6.9/8 6.6/4 6.4 6.4/2 6.6/6 7.1/12 7.6/13 7.6/14 7.3/15 6.9/20 5.6/24 5.1/30

6.1 6.1/2 6.2/13+FL 7.1/FL 5.9/20 5.6/30 2.9/H

2.8/30 3.0/76 2.9/20 3.1/17 6.1/12 6.1/11 6.6/10 5.8/9 5.5/4 5.3 5.3/2 5.5/6 5.8/10 6.3/11 6.1/13 5.3/20 4.3/24 3.7/27 3.8/30

1.2/30 1.4/24 1.6/21 2.0/19 5.2/12 5.8/11 5.7/10 4.6/9 3.9 3.8/2 4.1/8 4.3/10 4.9/11 4.2/12 4.0/13 2.3/16 2.6/20 2.2/30

Sta	+	H.I.	-	Elev	Rem	South — ℄ — North
		1116.97				
71+0						0.6/30 0.8/24 1.1/20 1.9/16 3.2/13 4.0/12 3.9/11 3.0/9 2.7/4 2.5 2.5/3 2.7/10 3.5/12 2.9/13 2.0/14 1.6/15 1.4/20 1.4/30
T.P.	9.22	1124.47	1.72	1115.25		(3.4/F.L. Drain at Sta 70+90)
72+0						6.1/30 6.3/27 6.5/23 7.0/19 7.7/15 8.9/13 9.7/12 9.6/11 8.8/10 8.1 8.0/2 8.3/7 8.6/11 9.2/13 8.4/14 7.5/16 7.4/18 7.6/25 7.4/30
73+0						4.6/30 4.6/26 4.5/20 5.2/17 7.1/13 7.7/12 7.1/10 6.7/9 6.2 6.2/2 6.5/7 6.8/10 7.1/11 6.7/13 5.9/15 5.8/23 6.8/30
+18	℄	Drive	North			5.8 5.7/2 6.0/7 6.7/12 6.0/25 6.0/30 (3.9/+1)
74+0						2.9/30 2.6/23 3.1/18 3.8/16 4.5/12 4.9/11 4.4/9 4.0/3 3.8 3.8/2 4.0/6 4.4/11 5.1/12 5.2/13 4.3/14 3.8/16 3.8/18 3.9/30 3.9/25
+36	℄	Drive	South			2.4/30 2.9/23 3.6/11 3.3
B.M. & T.P.	3.15	1126.10	1.52	1122.95 (1122.95 [illegible])		
75+0						(+0.4/4) 4.1/30 4.5/24 5.5/15 5.9/13 5.9/11 5.2/9 5.1/7 4.7 4.6/1 4.9/6 5.4/11 6.1/14 6.5/15 6.1/17 5.9/20 6.0/25 6.1/30
+44.2	℄	Culvert				5.6/17 6.4/15 7.6/13 8.0/F.L.* 3.6/10' 3.6/8.5 4.2/8.5 4.4/6 4.2 4.1/2 4.2/8.5 4.0/8.5 4.0/10' ← F.L. 8.1/F.L. 8.8/30' 9.1/100' 9.8/200' 10.7/300' 3.9/30 4.7/22 (7.2/F.L. Tile)
76+0						6.1/13 [illegible].9/12 6.9/11 5.9/10 5.0/9 4.7/8 4.9/7 4.7/4 4.6 4.5/2 4.7/6 5.0/10 5.2/12 5.9/14 6.5/16 5.9/17 5.8/19 5.6/22 5.9/30 2.8/30 2.9/28 3.5/24 4.1/20 5.4/14

OCT. 23, 1930 Windy

S. Gold Jr
S. Merritt
H. Barton

Sta	+	H.I.	−	Elev	Rems
		1126.10			
77+00					
78+00					
T.P.	10.73	1134.12	2.71	1123.39	
79+00					
B.M.			4.10	1130.02	
80+00					
T.P.	6.07	1138.67	1.52	1132.60	
81+00					
82+00					
T.P.	7.46	1143.02	3.11	1135.56	
83+00					
+20	℄	Drive	North		
84+00					

South ℄ North

1.1 1.4 2.5 4.8 5.1 5.7 5.2 5.0 4.5 4.1 3.9 4.3 4.6 5.4 5.4 5.1 4.3 4.6 4.8
28 25 20 16 14 13 12 11 9 8 7 10 12 13 15 18 26 30
0.9
30

3.1 4.3 4.6 4.7 4.1 3.7 2.8 2.6 2.6 2.9 3.4 4.3 3.4 3.3 3.2 3.6
20 18 17 15 14 13 11 6 5 9 11 12 14 19 30
1.7 2.4
30 26

9.2 9.4 9.5 10.2 10.1 10.5 9.9 9.4 9.1 9.1 9.3 9.6 10.2 10.1 10.0 9.6 9.2 8.9
30 27 22 21 19 17 15 12 6 4 5 9 11 12 15 17 24
8.7
30

5.3 6.5 6.8 6.4 4.9 5.4 6.2 4.7 4.3 6.0 6.2 6.4 7.5 7.7 6.7 4.0 4.0
21 20 19 18 17 13 11 9 5 4 8 10 11 13 17 27
3.8 3.7
26 30
2.2 2.3 3.3 4.2
30 29 27 24

4.3 4.6 5.4 6.9 7.3 7.0 6.2 6.3 6.3 6.4 6.7 7.0 7.7 7.2 6.0 5.3 5.3
30 26 21 17 16 14 12 10 5 5 7 9 11 13 16 21
5.1 4.9
25 30

2.7 3.1 3.8 4.8 5.6 5.7 5.1 3.8 3.5 3.5 3.9 4.3 4.9 4.3 2.8 2.8 2.7
27 24 19 17 16 15 14 12 3 5 8 10 14 19 30
2.6
30

5.4 5.1 6.0 6.4 8.8 9.1 8.8 6.8 6.6 6.6 6.9 7.1 7.0 5.8 5.6 5.7 5.7
30 28 24 20 17 16 15 12 6 8 12 18 18 25 30

6.3 6.8 6.3 6.0 5.8 5.6 3.5
9 16 24 29 30 H

5.0 5.1 6.9 6.4 5.3 5.1 5.0 4.9 5.2 5.3 5.7 6.4 5.7 5.8 6.7
24 20 18 17 15 14 10 3 3 7 8 9 23 30
5.7
25

Sta	+	HI	−	Elev.	Remarks
		1143.02			
84+80	℄ Culvert Inlet 85+	Channel than	Runs into West to	Rd Ditch culvert	2+42
85+0					
B.M.&T.P.	4.30	1145.38	1.92	1141.08 Rec 1141.10	
86+0	(6.7	Ditch 85+90)			
87+0					
T.P.	9.25	1153.12	1.51	1143.87	
88+0					
89+0					
T.P.	13.20	1164.58	1.74	1151.38	
90+0					
B.M.			4.48	1160.10	
91+0					
T.P.	8.40	1172.19	0.79	1163.79	
92+0					
T.P.	10.99	1181.68	1.50	1170.69	

South ℄ North

47/25 49/22 44/21 7.0/FL 2.9/17.4 2.9/15.4 3.9/15.4 4.1/14 3.7/5 3.7 3.7/1.7 2.8/1.7 2.8/3.5 FL 7.2 8.0/26 9.2/100
4.3/30

4.2/30 4.4/26 4.2/21 6.4/19 5.5/18 4.5/11 4.0/14 3.4/5 3.7 3.9/3 3.8/4.1 5.1/6 6.7/8 5.5/10 4.5/12 4.4/13 4.5/15
4.7/18 5.1/30

6.0/30 6.8/24 6.7/18 6.6/17 6.3/16 5.6/8 5.3/8 5.1/4 5.4 5.5/5 5.8/5 6.6/8 6.4/8 6.1/9 6.0/10 5.3/12 5.4/15 5.8/12
6.9/24 6.7/30

7.0/30 3.3/28 4.8/24 4.8/19 5.3/18 4.3/15 3.8/8 3.7/4 4.1 4.3/5 5.3/7 5.3/8 4.8/9 3.2/12 3.4/15 3.9/17 3.5/26
3.7/30

4.2/34 6.0/30 7.9/27 9.7/24 10.8/23 10.8/21 9.1/19 8.3/18 8.8 9.2/6 10.6/7 10.5/8 9.9/9 8.7/11 7.8/14 7.5/23 7.1/30
4.2/35

2.5/30 3.3/22 4.8/21 5.7/19 4.3/14 3.7/10 3.6/6 4.2 4.6/5 6.1/7 5.4/8 4.9/10 2.5/14 3.2/18 3.5/30

7.7/33 7.3/30 10.5/25 12.7/22 17.7/19 13.0/18 13.0/17 12.1/15 11.7/6 12.2 12.6/4 13.5/6 13.4/7 13.4/10 9.7/17 8.4/24 8.8/30

10.2/30 2.4/27 5.7/21 8.7/18 8.3/15 7.4/13 6.6/6 6.9 7.2/3 8.2/5 7.0/7 4.7/14 4.9/20 3.1/30

11.7/39 11.5/28 4.9/22 7.4/18 9.2/16 8.2/14 7.5/4 7.9 8.5/5 9.4/7 8.4/8 5.7/14 6.0/19 5.5/30

Sta	+	H.I.	−	Elev.	Remarks
		1181.68			
93+0					
94+0					
T.P.	8.82	1188.40	2.10	1179.58	
95+0					
96+0					
+83	℄	Drive	North		
97+0					
T.P.	6.71	1193.38	1.73	1186.67	
98+0					
B.M.			4.89	1188.49	
+53	℄	Culvert			
+74.7	℄	N & S. Road			

South ℄ North

45/30 43/24 84/18 125/18 108/12 105/9 10.7 110/5 115/2 109/7 87/10 74/14 78/18 75/30

09/30 07/26 11/23 30/17 41/14 53/13 40/11 39/2 4.1 47/6 52/8 31/10 28/14 33/8 30/30

40/30 46/27 42/25 70/18 74/15 83/14 72/12 7.1 77/7 82/8 63/12 66/16 67/30

31/30 34/24 37/18 55/13 54/12 47/11 4.3 49/6 53/8 51/9 47/12 47/25 50/30

3.1 35/7 40/12 50/30 (32/H)

26/30 26/22 26/17 32/15 38/13 32/11 3.1 33/7 41/14 34/23 34/30

58/30 69/23 60/19 63/15 72/14 71/12 68/11 6.4 65/3 72/8 79/11 74/13 69/20 73/30

48/109' FL 80/70S 49/19.5 51/19.5 5.1 62/15 64/15 54/16 88/FL 111/90'

34/100 49/30 49/15 5.4 60/14 74/30 93/90

Sta	+	H.I.	-	Elev	Rem's
		1193.38			
98+91	(Outlet Same as Culvert West)				
99+0					
100+0					
T.P.	7.18	1197.14	3.42	1189.96	
101+0					
102+0					
103+0					
104+0					
T.P.	10.78	1207.15	0.77	1196.37	
105+0					
106+0					

South ℄ North

49/100 79/FL 47/21 51/18 5.2 68/22 77/25 → E Ditch N 83 Road (87/FL) 104/100

42/30 45/28 58/24 71/23 74/20 71/18 64/12 49/11 50/9 5.0 51/4 55/11 60/13 71/14 72/17 60/18 62/30

24/30 26/25 28/19 39/17 40/14 55/11 60/10 60/9 49/8 4.5 44/3 48/8 52/11 54/12 51/14 43/16 40/25 42/30

44/30 49/23 52/17 73/12 82/10 89/9 88/8 77/7 7.1 70/5 75/10 78/13 81/14 77/15 69/19 64/26 65/30

33/30 37/25 39/18 51/13 66/10 74/9 74/8 61/7 5.6 54/4 59/10 67/12 66/13 63/15 55/17 55/25 55/30

24/30 28/25 27/18 30/15 37/13 46/11 56/10 37/9 3.3 32/5 38/12 51/14 41/15 36/17 39/26 43/30

0.6/30 0.9/26 1.0/19 1.8/13 2.4/10 3.5/9 2.4/8 2.1/6 1.7 1.6/5 2.1/10 3.0/15 1.9/17 2.8/24 3.0/27 3.3/30

35/30 9.0/24 9.0/18 8.7/13 10.9/11 11.2/8 10.4/6 10.1 10.0/5 10.4/10 10.8/12 11.3/14 11.1/16 10.0/25 10.0/30

43/30 45/27 46/21 53/15 86/11 9.2/9 89/8 8.2/6 7.8 76/4 83/11 9.1/14 18.2/15 76/20 66/26 64/30

Sta	+	H.I.	−	Elev	Rems
		1207.15			
107+00					
T.P.	12.00	1217.21	1.94	1205.21	
108+00					
109+00					
110+00					
111+00					
T.P.	7.93	1213.55	11.59	1205.62	
112+00					
B.M.			7.88	1205.67	
+50					
T.P.	0.92	1203.56	10.91	1202.64	
113+00					
+50					

South — ℄ — North

09/30 14/27 15/20 21/17 50/12 55/10 50/7 48/4 48 49/4 55/10 61/12 38/17 36/21 35/28 36/30

80/30 86/23 82/18 106/14 118/12 124/10 118/8 11.5 115/4 119/11 129/13 123/14 114/17 105/28 103/30

49/30 52/26 47/22 84/14 91/12 84/10 8.1 82/4 87/10 95/12 91/14 83/19 74/28 74/30

25/30 26/25 24/22 60/16 66/13 65/12 60/11 58/7 5.5 55/2 58/9 67/11 67/13 62/15 58/21 56/25 55/30

21/28 17/24 19/30 20/21 51/16 58/14 74/12 82/10 82/9 77/8 7.3 72/3 78/11 86/13 86/14 51/20 46/23 42/27 40/30

17/30 21/26 34/19 91/10 100/9 91/7 8.6 85/4 89/10 95/13 23/27 24/30

71/30 72/26 82/20 95/15 117/12 121/11 130/10 127/9 120/7 11.7 116/5 123/13 139/16 126/17 108/22 95/24 91/30

13/30 19/27 24/18 50/11 61/9 67/8 55/6 5.8 52/5 55/11 58/14 63/16 63/19 49/23 33/27 34/30

42/28 57/24 70/15 86/10 89/9 93/8 86/7 85/6 8.1 98/5 81/14 96/17 93/21 81/25 77/30 47/30

Sta	+	H.I.	−	Elev.	Items
		1203.56			
114+0					
T.P.	5.80	1198.54	10.82	1192.74	
+18					
T.P.	6.86	1199.82	5.58	1192.96	
+66					
+72.5					
+89.5	℄	Bridge			
115+02.4					
+08.4					
+50					
116+0					
T.P.			1.56	1198.26	

South ℄ North

10.8/30 10.5/24 11.0/18 11.3/13 10.4/9 9.7/7 9.5 9.3/4 9.9/11 11.0/14 11.1/17 10.5/20 10.8/26 10.8/30

10.9/30 10.5/22 9.0/15 4.9/8 4.6 4.5/3 5.0/11 7.0/18 8.9/28 9.6/30

6.1/16.3 6.7/18.4 8.2/15.7 7.7/13 6.2/8 5.9 6.4/8 13.0/18

6.1/16.6 6.1/15.7 7.6/15.7 6.7/13 6.3/9 5.9 6.3/9 8.0/10.0 6.9/10.0 6.85/10.9

6.1/17.9 6.1/17.0 7.7/17.0 6.6/14.0 6.3/10 5.8/5 5.8 6.2/2 7.3/9.1 6.7/9.1 6.2/10.0

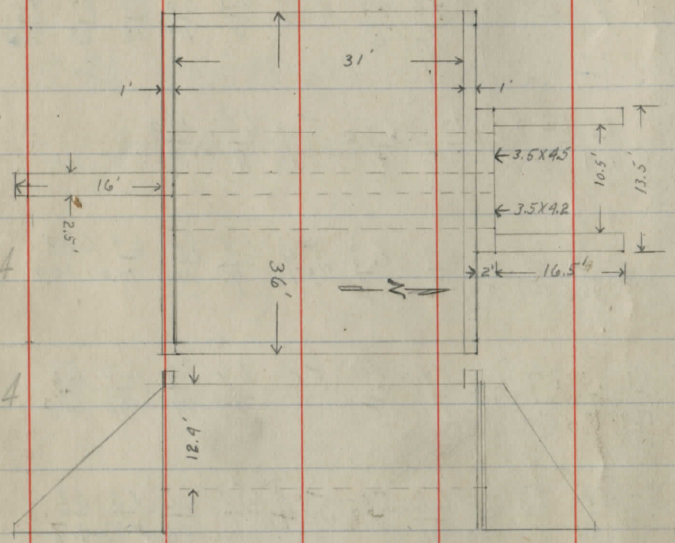
6.3/18.9 6.3/18.0 7.5/18.0 6.6/12 5.9/9 5.4 5.9/2 6.6/8.8 6.3/8.8 6.2/9.7

12.8/21 10.2/19.0 5.7/10 5.3 5.8/6 7.5/8.3 6.3/8.3 6.3/9.2

12.8/30 11.9/22 9.6/21 6.1/13 4.1/9 3.9 4.2/7 7.8/11 11.6/19 12.3/21

5.0/30 4.5/25 5.7/24 3.8/20 3.2/15 1.5/10 1.2 1.6/7 4.2/13 5.7/20 6.2/21 9.4/26 10.7/30

Sta	+	H.I.	−	Elev.	Rem's
T.P.	1.12	1186.92		1185.80	
114+66					
+72.5					
+89.5					
115+02.4					
115+08.4					
+50					
T.P.	1.26	1187.70		1186.44	
114+66					
+72.5					
+89.5					



South ℄ North

5.3/22 6.2/28 6.5/30

0.7/14 3.5/19 7.4/24 7.7/30

11.3/13 or FL 11.2/15 11.9/15 12.0/17 13.6/17 13.4/18 16.8/18

4.7/125 7.8/22 8.5/30

0.0/13.0 4.2/22 7.3/30

1.1/30

7.0/30 6.4/195

8.3/30 8.1/20

9.1/33 11.4/21.5 or FL

Sta	+	H.I.	−	Elev	Rem's
		1187.70			
116+024					
+08.4					
T.P.	9.06	1207.32		1198.26	
116+35					
T.P.	11.72	1217.75	1.29	1206.03	
117+0					
B.M.	7.90	1225.57	.10	1217.65	1217.67 adjd
117+90		Also drive North			
118+0					
T.P.	13.23	1237.35	1.45	1224.12	
119+0					
120+0					
T.P.	11.36	1248.14	0.57	1236.78	
121+0					

South — ℄ — North

8.2/30 7.8/26 4.2/22

5.9/30 4.5/26 0.7/21

4.5/30 4.3/25 5.8/21 7.9/16 8.8/12 6.8/9 6.2 6.5/8 7.9/11 7.7/14 8.5/20 9.5/27 9.4/30

1.0/30 3.7/23 11.6/14 12.7/12 11.6/10 11.5 11.7/5 12.1/8 12.8/9 10.2/14 10.1/17 8.3/21 7.2/27 7.1/30

1.1/30 1.3/25 2.8/21 9.3/14 10.4/13 9.8/11 9.8 9.7/6 9.4/9 9.9/F2 8.7/20 8.8/30

0.7/30 1.2/24 2.2/22 6.9/17 8.0/15 9.6/13 8.7/12 8.7 8.6/6 9.8/8 7.4/11 6.8/14 6.3/19 4.6/25 2.9/27 3.0/30

6.7/30 7.2/22 8.7/19 10.1/18 11.5/15 12.9/14 11.7/12 11.4/4 11.5 11.7/4 12.0/8 12.6/9 11.6/11 8.3/15 8.4/22 8.5/24 7.9/30

0.7/30 1.7/27 2.1/20 3.2/16 5.5/14 4.4/12 4.1 4.3/5 4.8/9 5.5/10 4.8/12 1.7/15 1.7/18 2.1/21 2.4/26 2.5/30

4.5/27 6.6/21 7.6/17 8.0/16 8.9/14 9.8/13 9.4/12 9.0/10 8.7/8 8.5 8.7/5 9.1/10 10.1/11 9.1/12 7.1/15 7.1/18 7.7/21 7.7/26 7.6/30 6.7/30

Sta	+	H.I.	−	Elev.	Rem's
		1248.14			
122+0					
T.P.	11.45	1258.51	1.08	1247.06	
123+0					
B.M.			5.88	1252.63	
+64	℄ Drive South				
124+0					
+86	℄	Drive	North		
125+0					
126+0					
T.P.	3.15	1256.51	5.15	1253.36	
127+0					
+07	℄ Drive South				

South ℄ North

1.3/30 1.5/20 2.2/17 3.7/12 4.1/10 3.7/9 3.6 3.5/3 4.0/10 4.6/12 2.3/16 2.3/19 2.6/21 2.3/26 1.9/28 1.9/30

8.1/30 8.0/21 8.3/16 9.2/14 9.9/10 10.2/9 10.2/8 9.9/7 9.5 9.4/5 9.6/8 10.2/13 9.8/16 9.0/18 8.9/21 8.6/26 8.4/30

1255.0 → 3.5/21 6.8/30 7.0/25 7.8/8 7.3

5.1/30 5.0/22 4.9/15 5.6/12 6.8/9 6.1 5.9/4 6.1/11 6.1/12 5.9/15 5.7/21 5.2/24 4.8/28 4.6/30

4.3 4.3/4 4.7/13 4.2/16 4.3/27 4.5/30 2.9/H

3.9/30 4.0/22 4.4/14 5.1/9 4.9/7 4.5 4.5/3 5.0/13 4.9/19 4.1/25 3.6/30

5.3/30 5.4/19 5.7/14 6.0/11 5.7/7 5.3 5.3/4 5.6/11 6.1/13 5.7/14 5.6/21 5.4/25 5.4/30

3.6/30 3.8/21 4.0/13 4.7/10 4.0 4.0/5 4.3/11 4.9/15 4.3/17 4.1/22 3.9/27 3.9/30

4.1/30 4.2/18 4.6/11 4.4/6 4.1

Oct 27, 1930 (Fair)

S. Gold Jr
S. Merritt
H. Barton

Sta	+	H.I.	−	Elev	Rem's	South	℄	North
		1256.51						
128+0						4.5/30 4.5/19 5.3/12 6.2/9 5.9/7	5.4	5.4/4 5.7/11 6.2/14 6.1/15 5.2/18 5.2/19 5.1/22 4.8/24 4.4/30
129+0						6.8/30 6.8/27 7.1/21 7.7/14 8.0/12 7.7/9	7.2	7.4/10 7.6/13 7.9/14 7.9/15 6.8/20 6.3/28 6.6/30 (4.1/H) 1252.4
B.M. & T.P.	2.57	1252.13	6.97	1249.56 [illegible] 1249.54				
+26 ℄ Drive North							3.1	3.3/11 3.7/14 2.8/23 2.6/30
130+0						4.4/30 4.2/27 4.3/18 4.5/13 5.3/11 4.2/8	3.9	3.9/6 4.2/12 4.5/13 5.1/15 5.0/16 4.9/17 4.3/21 4.3/26 4.4/27 4.5/30
131+0						5.8/30 5.6/18 5.3/13 6.4/11 5.5/10	5.0	5.1/6 5.3/13 6.1/15 6.7/16 6.0/17 5.3/22 5.4/27 5.9/28 5.8/30
132+0						6.0/30 6.2/18 6.0/15 5.6/14 6.3/12 6.9/11 6.1/10 5.4/9	5.1	5.1/6 5.5/12 7.1/16 7.3/17 6.5/18 5.4/22 5.5/27 6.4/28 6.1/30
+73.5 ℄ Culvert						6.6/30 6.7/17 7.2/FL→ 3.5/10.8 3.5/8.8 5.0/8.8	4.5	4.6/7 4.2/12.5 3.6/12.5 (1248.4) 3.7/14.0 ← 7.2/FL (44.9) 7.2/17 5.4/20 5.5/22 5.6/27 6.5/28 6.4/30
T.P.	3.93	1252.52	3.54	1248.59				
133+0						6.4/30 6.5/19 6.2/14 7.2/12 6.2/10 5.2/8	5.0	5.0/5 5.2/11 5.0/12 7.0/14 7.6/17 7.0/19 6.0/22 6.1/28 7.1/29 6.8/30
+45 ℄ Outlet Ditch						5.6/200 6.1/100 6.3/27 6.4/19 5.7/14 6.5/13 6.5/11 5.4/9	5.0	5.2/11 5.6/13 7.3/16 8.4/21 (5.2/PB) 8.3/28 8.4/100 8.7/140 9.3/141 9.7/200 10.0/300

(4x12 Plank Bridge over Outlet Channel)

Sta	+	H.I.	−	Elev	Rems
		1252.52			
134+0					
135+0					
136+0					
137+0					
T.P.	9.30	1260.47	1.15	1251.37	
138+0					
139+0					
140+0					
T.P.	7.63	1265.75	2.55	1258.12	
141+0					
B.M.			6.03	1260.72	

140+0 (F.L Stone Pipe (4.6))

+ 20 ℄ Drive South

South ℄ North

60/30 59/20 52/12 45/11 54/9 5.0 52/11 54/14 71/17 67/19 55/22 55/27 63/30

54/30 51/23 52/17 52/13 56/11 48/9 4.4 47/11 50/13 57/15 61/17 58/18 57/20 50/22 51/27 58/29 59/30

47/30 43/23 40/15 46/12 43/11 40/9 3.7 39/11 42/13 53/15 51/18 41/21 43/22 43/26 42/27 50/30

25/30 26/23 30/14 34/12 35/11 30/10 2.9/9 2.5 28/13 37/15 41/16 35/17 34/19 27/22 27/26 27/30

83/30 85/25 92/19 93/14 104/11 85/9 9.1 90/10 94/13 102/15 99/16 89/21 84/23 82/27 83/30

58/30 66/27 74/14 82/12 73/10 75/8 7.3 71/5 74/10 82/11 75/16 59/21 60/26 61/30

57/30 (74/FL+) 62/14 67/8 6.6

18/30 18/25 34/19 48/14 55/13 44/10 4.1 45/11 37/11 30/20 30/24 30/30

59/30 57/24 61/18 87/14 76/10 7.2 75/10 63/15 62/25 61/25 59/30

Sta	+	H.I.	−	Elev.	Cent'l
		126575			
141+30	℄	Drive North			
142+0					
143+0					
144+0					
T.P.	5.95	1267.71	2.99	1261.76	
+30	℄	Drive North			
+67	℄	Drive South			
145+0					
146+0					
+09	℄	Drive North			

South ℄ North

80/82 Stone Pipe 14' off ℄

6.6 65/9 61/21 59/25 58/30 (47/H)

49/30 49/23 47/18 58/14 63/12 70/11 60/9 55/4 5.4 55/5 59/7 67/13 68/14 54/16 50/20 51/25 46/28 48/30

50/30 49/20 51/14 64/12 48/9 43/3 4.2 43/5 48/11 60/13 49/14 48/16 51/18 45/20 45/25 49/26 49/30

43/30 43/21 44/16 47/15 58/13 53/12 44/10 4.0 40/4 43/10 53/12 46/14 42/15 48/17 45/18 41/20 41/22 40/26 42/30

5.7 59/9 71/12 61/14 60/22 59/30 (55/H)

GFL Plank O.F

60/30 60/20 59/10 5.6

53/30 53/25 53/20 58/12 67/12 57/9 5.4 53/4 57/10 65/12 60/13 53/16 54/21 54/24 51/30

48/30 49/24 51/19 49/16 51/14 53/13 55/14 50/10 4.5 46/4 51/10 56/14 50/13 45/19 46/24 47/30 (46/H)

4.4 48/8 51/12 ← FL 56/18 48/22 45/30 45/30

Sta	+	H.I.	−	Elev	Rem's
		1267.71			
147+0					
+88	℄	Drive South			
148+0					
149+0					
T.P.	12.69	1278.53	1.87	1265.84	
+87	℄	Drive North			
150+0					
				1271.80	
B.M.			6.73	1271.80	
151+0					
+15					
+57	W. Edge Pave				

South ℄ North

37/30 38/27 40/15 49/13 41/11 3.7 37/3 40/9 47/11 44/12 39/14 36/17 32/19 32/25 33/30

1.1/H 24/30 27/15 3.3/FL 26/13 24/11 2.1

20/30 20/20 27/15 31/13 25/11 2.0 26/8 32/10 27/12 28/18 23/20 22/24 20/27 21/30

20/30 18/17 17/15 19/13 15/11 12/5 1.1 15/8 20/11 17/12 17/17 15/19 15/24 1.4/30

10.5 109/7 112/13 108/16 105/23 10.1/30

100/30 10.2/28 109/23 107/15 108/13 108/11 104/7 10.3 105/6 109/10 104/15 10.2/20 98/24 9.6/30

5.5/25' 59/30 Alla Pump 61/25 70/17 76/13 83/11 78/3 7.9 82/6 83/8 80/10 84/FL Drain 11' 67/15 64/19 59/23 55/27 57/30

7.15/50 N.E. Pave 67/36 67/31 65/30 63/27 69/13 73/12 74/11 7.1 77/7 60/27 59/30 51/H

7.88/75' Pave 8.42/97' Pave

64/30 63/27 69/26 70/24 67/27 60/20 5.80/18' S.E. Pave 5.41/10 5.4 5.65/3 C N.E. Pave 51/14 49/24 44/30

Sta	+	H.I.	−	Elev.	Rem'k
		1278.53			
151+80					
152+0					
+11.48	℄	Road	Running	North (ACH # 377) 1276.27 adj.	
B.M.			2.27	1276.26	

South ℄ North

39/30 43/20 48/19 54/16 58/14 5.52/12 5.07/9' ℄ SE Face 4.68 4.76/9' → N.E. Row 4.9/12' 4.9/27' 4.7/30

34/30 35/26 40/20 46/14 44/10 415/6' 4.03/4' ℄ Edge Row 3.98 4.00/12' ↳ Edge Face 4.1/17' 4.1/30

36/30 36/23 41/13 36/5 3.54/2' ℄ Edge Row 2.52 3.59/9' 3.71/15' 4.05/19' ★ Conc Face 4.11/34' 4.39/100'

Thompson-Leroy Rd. June 5, 1931.

Sta	+	H.I.	−	Elev.	Remks
B.M.	3.49	1073.48		1069.97	#1
0+0					
0+50					
1+0					
2+0					
3+0					
T.P.	7.15	1078.78	1.85	1071.63	
4+0					
5+0					
B.M.	3.58	1078.76	3.58	1075.18 1075.20	B.M. #2
6+0					
7+0					

Fair "SLOPE STAKES" S. Gold St. S. Merritt

North	℄ Elev.	South
	1067.27	
C. 1.5 24.0'	1068.18	C. 1.0 23.0'
C. 1.5 23.7'	1068.65	C. 2.5 25.3'
F. 4.0 22.0'	1069.15	F. 3.0 20.7'
C. 2.0 28.3'	1070.00	F. 1.0 24.7'
C. 1.0 22.9'	1072.73	C. 0.5 22.0'
C. 0.5 22.3'	1074.38	F. 0.5 20.5'
C. 0.5 22.1'	1074.85	Gr. 21.1'
Gr. 21.5'	1075.15	Gr. 20.9'

Sta	+	H.I. 1078.76	-	Elev	Remarks
8+00					
T.P.	5.14	1080.59	3.31	1075.45	
9+00					
10+00					
B.M.			3.67	1076.92	B.M. #8
11+00					
12+00					
13+00					
T.P.	4.65	1080.55	4.69	1075.90	
14+00					
15+00					
16+00					

North	± Elev.	South
F. 0.5 / 21.3'	1075.45	Gr. / 21.0'
F. 0.5 / 21.3'	1075.75	Gr. / 21.3'
Gr. / 21.7'	1076.05	Gr. / 21.7'
Gr / 21.7'	1076.35	Gr. / 21.7'
F. 0.5 / 21.1'	1076.58	Gr. / 21.3'
F. 0.5 / 20.9'	1076.40	F. 0.5 / 21.3'
F. 0.5 / 21.1'	1076.15	Gr. / 21.3'
F. 0.5 / 21.3'	1075.90	C. 0.5 / 22.1'
C. 0.5 / 22.5'	1074.96	C. 1.0 / 23.5'

Sta	+	H.I.	-	Elev.	Rem's
		1080.55			
17+0				1074.25	
B.M.	3.45	1077.70	6.33	1074.22	B.M.#4
18+0					
19+0					
20+0					
B.M.	3.91	1077.16		1073.25	
20+25					
21+0					
22+0					
23+0					
	5.04	1078.29	3.91	1073.25	
23+68.38		3.03			

North		℄ Elev.		South
C.0.5 / 21.9'		1073.86		C.1.5 / 23.9'
F.1.5 / 19.5'		1077.40		F.2.0 / 19.0'
C.0.5 / 22.0'		1072.42		Gr. / 21.3'
Gr. / 20.7'		1074.86		C.1.0 / 22.9'
F.0.5 / 21.0'		1075.26		C.0.5 / 22.7'
Gr. / 21.9'		1074.46		C.1.0 / 23.3'
F.1.0 / 20.1'		1073.06		Gr. / 21.5'
F.1.0 / 20.3'		1071.66		F.1.0 / 20.5'
F.1.0 / 21.0'	1072.03		1071.37	C.1.0 / 26.0'

Sta	+	H I	-	Elev	Rem's
		1078.79			
24+0		5.11			
24+25		5.60			
24+50		5.60			
24+75		5.60			
	26	1080.87	5.04	1073.25	
25+0		5.60			
25+25		5.41			
25+50		4.20			
+45.3 P.T.		3.03			
26+0		.40			

North		South
1077.88	Intersection	C. 1.5 / 29.3' — 1071.81
1073.62	F. 1.5 / 20.0	C. 3.0 / 31.5' — 1077.31
1074.12	F. 1.5 / 18.5'	C. 3.0 / 37.0 — 1077.81
1074.62	Gr. / 21.3	C. 3.0 / 37.0 — 1073.31
1075.12	F. 0.5 / 21.5'	C. 3.0 / 31.5 — 1073.81
1075.47	Gr. / 21.7'	C. 2.5' / 31.0' — 1074.29
1075.60	Gr. / 21.5'	C. 2.5' / 29.3' — 1074.75
1075.66	Gr. / 21.7'	C. 2.0 / 27.7' — 1075.00
1075.66	Gr. / 22.3'	C. 1.5 / 25.0 — 1075.46

Sta	+	H.I	-	Elev.	Rem's
		1080.87			
27+0					
28+0					
29+0					
T.P.	6.67	1084.41	3.13	1077.74	
30+0				1080.47 Rec'd	
B.M.			3.94	1080.47	
31+0					
	4.74	1085.21		1080.47	
32+0					
T.P.	7.32	1087.91	4.62	1080.59	
33+0					
33+53.60	P.C.				
+75					

North		℄ Elev.		South
Gr. 21.3'		1076.96		C.0.5 22.1'
F.1.0 20.5		1077.86		F.0.5 21.1'
F.1.0 20.1		1078.74		Gr. 21.5
F.1.0 20.3		1079.53		F.1.0 20.3
F.1.0 20.1		1080.30		F.0.5 21.1'
F.0.5 20.9		1081.09		Gr. 22.1'
Gr. 21.7'		1082.36		C.0.5 22.5'
C.0.5 23.0	1082.97		1082.65	C.1.5 24.5'
C.0.5 23.0	1083.29		1082.53	C.2.0 25.5'

Sta	+	H.I.	−	Elev.	Rem's
		1087.91			
34+0					
34+25					
34+50					
P.T. +80.98					
35+0					
36+0					
37+0	?			1085.61 rec.	
B.M.	5.20	1090.81	7.33	1085.58	
38+0					
39+0					
T.P.	6.12	1093.77	3.16	1087.65	

North		℄ Elev.		South
C.0.5 / 23.5'	1083.62		1083.01	C.2.5 / 25.5'
C.0.5 / 23.5'	1083.81		1083.18	C.1.0 / 24.0'
C.0.5 / 23.0'	1083.65		1083.34	C.1.5 / 23.5'
C.0.5 / 23.7'	1083.87		1083.50	C.1.0 / 23.5
Gr. / 22.0'	1083.80		1083.61	C.0.5 / 23.5
F.1.0 / 20.5		1084.26		F.1.0 / 20.3'
F.1.0' / 20.3		1085.01		F.0.5' / 20.7'
Gr. / 20.5		1086.26		Gr. / 21.7'
Gr. / 21.5		1087.65		C.0.5 / 22.7'

Sta	+	H.I.	-	Elev	Rem's
		1093.77			
40+0					
41+0					
42+0					
T.P.	5.47	1096.13	3.11	1090.66	
43+0				1092.43 Rec.	
B.M.			3.69	1092.44	
44+0					
45+0					
46+0					
T.P.	6.16	1100.08	7.21	1093.92	
47+0					
48+0					
B.M.			3.62	1096.46	

North	℄ Elev.	South
C. 0.5 / 21.7'	1088.63	C. 0.5 / 22.3'
C. 0.5 / 22.7'	1089.15	C. 1.0 / 23.1'
C. 0.5 / 22.5'	1090.16	C. 0.5 / 22.5'
Gr. / 21.5'	1091.21	C. 0.5 / 22.0'
C. 0.5 / 22.1'	1091.93	Gr. / 22.0'
C. 1.0 / 22.7	1092.39	C. 0.5 / 22.3'
C. 1.0' / 22.7'	1092.92	C. 1.0 / 22.5'
C. 0.5 / 22.3	1094.06	Gr. / 22.0
Gr. / 21.7'	1095.30	C. 0.5 / 22.0'

Sta	+	H.I.	-	Elev.	Rem's
		1100.08			
49+0					
50+0					
T.P.	7.70	1105.48	7.30	1097.78	
51+0					
52+0					
53+0					
54+0					
T.P.	5.42	1109.37	1.53	1103.95	
55+0					
55+50					
56+0					

North	℄ Elev.	South
C.0.5 / 22.3'	1096.54	C.0.5 / 22.5'
Gr. / 21.7'	1097.78	C.1.0 / 22.3
C.0.5 / 22.1	1099.07	C.1.0 / 23.1'
C.1.5 / 23.7'	1100.26	C.1.5 / 23.7'
C.0.5 / 27.0'	1101.50	C.0.5 / 22.5
C.0.5 / 22.7	1102.74	C.1.0 / 23.1
Gr. / 22.0'	1103.98	C.0.5 / 22.7
C.0.5 / 22.3'	1104.42	C.1.0 / 22.5
F.0.5 / 21.1'	1104.50	C.0.5 / 22.3

July 7, 1931

S. Gold Jr.
S. Merritt
H. Chapman

Sta	+	H.I.	−	Elev	Rems
		1109.37			
57+00					
58+00					
T.P.	7.40	1113.36	3.41	1105.96	
59+00					
B.M.		1113.32	5.88	1107.48	1107.44 rec
60+00					
61+00					
62+00					
	5.80	1115.52		1109.72	
63+00					
+36.56	P.C.				INTERSECTION
+50					

North		℄ Elev		South
F 1.0 / 20.7'		1104.39		F 0.5 / 23.0'
F 2.0' / 21.0'		1104.87		F 1.5 / 21.0'
F 1.0 / 20.0'		1106.02		F 1.5 / 20.1'
C 0.5 / 22.3		1107.49		C 1.0 / 24.5
C 0.5 / 22.1'		1108.77		C 1.0 / 23.5
Gr / 21.7'		1109.72		C 1.0 / 23.1'
Gr. / 22.0'	1110.11		1110.02	
	1110.61		1110.09	
	1110.52		1110.12	

Sta	+	H.I	−	Elev.	Rem's
		1115.5✓			
64+0					
T.P.	4.5✓	1114.8✓	5✓	1110.30	
+50					
65+0					
+50					
66+0					
+50					
T.P.	4.6✓	1116.06	3.38	1111.44	
67+0					
+48.70	P.T.		4.36	1111.70 rec. ✓ 1111.70	
B.M.					
68+0.					

North		℄		South
F.1.0 / 21.1	1110.85✓		1110.22✓	C.0.5 / 22.5
Gr. / 21.7'	1110.95✓		1110.32✓	C.0.5 / 23.3
F.0.5 / 21.7'	1111.05		1110.4✓	C.1.0 / 23.0'
F.1.0 / 21.0'	1111.15		1110.5✓	C.1.0 / 23.3'
F.1.5 / 21.0'	1111.23		1110.60	Gr. / 21.7'
F.2.0 / 20.3'	1111.18		1110.55	F.0.5 / 21.1'
F.1.0 / 20.5'	1111.14		1110.51	F.1.0 / 21.8'
F.1.0 / 20.7'	1110.89		1110.57	F.0.5 / 21.1'
Gr. / 21.0'		1110.8✓		F.0.5 / 21.3'

Sta	+	H. I.	−	Elev.	Cents
		1116.06			
69+0					
T.P.	7.18	1119.46	3.78	1117.28	
70+0					
71+0					
72+0	2 See	Section			
T.P.	8.20	1125.64	2.02	1117.44	
73+0					
74+0					
74+25					
B.M.			2.69	1122.95	
75+0		18" × 30" Ditch			
76+0					

North	℄ Elev.	South
Gr. 21.3'	1112.07	C. 2.0 / 25.0
C. 1.0 / 23.3'	1113.67	C. 2.0 / 24.7'
C. 0.5 / 22.3'	1115.27	C. 1.0 / 23.1'
C. 0.5 / 22.4'	1116.93	C. 1.5 / 23.5'
Gr. / 21.5'	1118.97	C. 1.0 / 23.0
Gr. / 21.5'	1121.07	C. 1.0 / 23.1'
F. 0.5 / 21.3	1121.44	C. 1.0 / 22.9'
F. 1.0 / 22.5'	1121.20	C. 0.5 / 24.1'
F. 1.0 / 22.3'	1121.57	C. 1.5 / 25.5'

Sta	+	H.I.	-	Elev	Remr	North	℄ Elev.	South
		1175.64						
77+0						F.1.0 / 20.5'	1172.74	S.2.0 / 24.0'
T.P.	5.36	1130.08	0.94	1124.72				
78+0						F.1.0 / 20.5'	1173.94	F.0.5 / 22.0'
79+0						F.0.5 / 21.3'	1175.53	F.0.5 / 23.0'
B.M.	3.70	1133.70	0.05	1130.03	1130.00			
80+0						C.1.5 / 23.5'	1179.04	C.1.0 / 23.0'
T.P.	7.96	1139.82	1.14	1132.06				
81+0						C.1.0 / 22.7'	1137.82	C.0.5 / 22.0'
+50						C.0.5 / 22.3'	1134.42	C.0.5 / 21.7'
82+0						C.0.5 / 22.5'	1135.47	Gr. / 21.0'
83+0						C.0.5 / 22.7'	1136.82	Gr. / 21.7'
84+0						F.1.0 / 20.7'	1138.22	Gr. / 21.7'
T.P.	6.75	1144.97	1.60	1138.22				

Sta	+	H.I.	−	Elev.	Remarks
		1144.97			
85+0					
86+0					
B.M.			3.93	1141.08 Rec. 1141.04	
87+0					
T.P.	7.97	1147.44		1139.57	
87+50					
88+0					
T.P.	11.75	1158.73	0.47	1146.97	
89+0		See Section			
90+0					
T.P.	7.66	1164.27	2.17	1156.61	
91+0		See Section			
B.M.	4.20	1164.30	4.20	1160.10 1160.07	
92+0					
T.P.	12.51	1176.40	0.41	1163.89	

North	± Elev.	South
F.1.5 / 20.5	1139.67	F.1.0 / 23.0'
F.1.5 / 20.0'	1141.02	F.2.0 / 20.0'
F.0.5 / 21.3'	1142.42	F.2.0 / 21.3'
	1143.41	
C.1.0 / 22.5	1144.98	F.1.0 / 24.5'
C.2.0 / 24.1'	1148.70	C.1.5' / 25'
C.3.0 / 25.9'	1153.14	C.2.5 / 26.0'
C.2.5' / 25.5'	1159.07	GT / 23.0
C.1.0 / 22.9'	1165.67	C.3.5 / 24.5'

Sta	+	H I 1176.20	−	Elev	Rem's	North	℄ Elev.	South
T.P.	8.98	1184.02	1.36	1175.04				
93+0						C. 2.0' / 24.7'	1177.22	C. 5.0' / 29.5'
94+0						C. 1.0 / 22.9'	1177.92	C. 3.5 / 26.0'
T.P.	7.57	1186.42	3.17	1180.85				
95+0						Gr. / 22.0'	1181.82	C. 2.5 / 24.3'
96+0						F. 0.5 / 20.7'	1184.61	C. 0.5 / 22.3'
97+0						F. 1.0 / 19.7'	1186.12	Gr. / 21.5
98+0						F. 0.5 / 20.5'	1187.42	Gr. / 21.9
T.P.	6.37	1193.29	1.50	1186.92				
99+0		INTERSECTION		1188.49		F. 0.5 / 20.3	1188.68	F. 0.5' / 26.5'
B.M.		1193.33	4.84	1188.45				
100+0						F. 0.5 / 21.1'	1189.72	C. 1.0 / 23.5'
T.P.	5.39	1196.11	7.61	1190.72				
101+0						Gr. / 21.3	1190.72	C. 2.0 / 24.3'

Sta	+	H.I.	-	Elev.	Rem's
		1196.11			
102+0					
103+0					
T.P.	7.39	1200.96	2.54	1193.57	
104+0					
105+0					
T.P.	12.10	1208.97		1196.87	
106+0					
107+0					
108+0					
T.P.	10.86	1217.18	2.65	1206.32	
109+0					
110+0					

North	℄ Elev.	South
F.0.5 / 21.1'	1192.17	C.1.5 / 23.7'
F.0.5 / 21.0'	1194.07	C.0.5 / 22.3'
F.1.0 / 20.7'	1195.97	Gr. / 22.3'
F.1.0 / 20.1'	1197.87	C.0.5 / 22.5'
Gr. / 20.9'	1200.42	C.2.5 / 25.5'
Gr. / 22.0'	1203.62	C.2.0 / 25.1'
F.0.5 / 20.9'	1206.82	C.2.0 / 25.0
F.1.0 / 20.5'	1210.02	C.2.5' / 25.5'
Gr. / 21.7'	1211.67	C.3.0' / 26.5'

Sta	+	H.I.	-	Elev.	Remks
		1217.18			
111+0					
111+50					
112+0					
T.P.	0.52	1217.72	5.48	1211.70	
113+0	Slope 2:1 North Side				
B.M.			6.52	1205.70	1205.22 ±
114+0					
T.P.	0.93	1201.59	11.56	1200.66	
115+0					
T.P.	8.04	1202.11	7.52	1194.07	
116+0					
T.P.	12.18	1214.20	0.09	1202.02	
117+0					
T.P.	7.51	1220.00	1.71	1212.49	
118+0					
B.M.	10.68	1228.35	7.32	1217.67	1217.67 Rec. 1217.68

North	℄ Elev.	South
C. 3.0 / 75.7	1210.22	C. 5.0 / 29.3
C. 5.0 / 79.5'	1208.34	C. 7.0 / 32.0
C. 5.5' / 30.3'	1205.70	C. 6.0 / 31.1'
C. 1.0 / 28.0	1199.66	C. 2.0 / 25.0
F. 1.5 / 20.0	1194.95	F. 2.0 / 22.0
	1194.79	
F. 10.5 / 32.0	1199.79	F. 4.0 / 23.0
C. 1.5 / 23.3'	1208.62	C. 8.0 / 32.0'
C. 5.0 / 27.0	1217.62	C. 7.5 / 32.0'

Sta	+	H.I. 1228.35	−	Elev	Remarks
T.P.	5.85	1233.64	0.56	1227.79	
119+0					
T.P.	17.87	1241.99		1224.12	
119+50					
120+0					
T.P.	13.10	1253.92	1.17	1240.82	
121+0					
122+0					
123+0					
B.M.	6.52	1259.16	1.28	1252.64 1252.64 Rec.	
124+0					
124+50					
125+0					

North	Elev.	South
C. 2.5 / 25.5'	1226.62	C. 4.5' / 28.0'
C. 1.0 / 23.5'	1230.72	C. 1.0 / 23.3'
C. 1.0 / 23.0	1234.02	C. 2.0' / 27.0
C. 1.0' / 22.7	1239.82	C. 2.0 / 24.5'
C. 0.5 / 22.3'	1245.62	C. 1.0 / 23.5'
G. / 22.0'	1249.62	C. 1.0 / 23.3'
C. 0.5' / 22.0'	1252.77	C. 1.0 / 23.5'
C. 1.5' / 23.5'	1253.71	C. 1.5 / 22.5'
G. / 21.3'	1254.22	C. 0.5 / 22.5'

Sta	+	H.I.	−	Elev.	Rem's
	3.03	1259.25		1256.22	
126+0					
127+0					
128+0					
T.P.	7.39	1254.56	5.08	1252.17	
129+0				1249.56	
B.M.		1254.54	4.98	1249.58	
130+0					
131+0					
T.P.	4.54	1250.91	8.17	1246.37	
132+0					
133+0					
133+50					

North	℄ Elev.	South
F. 1.0 / 20.3'	1253.97	F. 0.5 / 20.7
Gr. / 21.3'	1252.87	Gr. / 21.7'
Gr. / 21.5'	1251.68	C. 0.5' / 22.5'
Gr. / 21.5	1249.97	Gr. / 21.3'
F. 0.5' / 20.5'	1248.36	Gr. / 21.3'
F. 1.5 / 20.0'	1247.87	F. 1.5' / 20.0'
F. 0.5 / 22.0'	1247.57	F. 1.0 / 19.91
F. 0.5 / 22.5'	1247.45	F. 1.0 / 21.5'
	1247.53	

Sta	+	H.I.	−	Elev.	Rem's
		1250.91			
134+0					
135+0					
T.P.	8.16	1255.98	3.09	1247.82	
136+0					
137+0					
138+0					
139+0					
T.P.	9.68	1263.85	1.81	1254.17	
140+0					
140+50					
141+0					
B.M.				1260.73	

North	℄ Elev.	South
F 0.5 / 23.0'	1247.70	F 1.0 / 21.3'
F 1.0 / 22.0'	1248.32	F 0.5 / 20.5'
F 0.5 / 22.0'	1249.12	F 0.5 / 20.5'
F 0.5 / 20.5'	1250.22	Gr. / 21.3'
C 0.5 / 22.7'	1251.92	C 0.5 / 21.7'
C 1.0 / 23.0'	1254.17	Gr. / 21.5
C 1.0 / 23.3'	1256.92	C 2.0 / 24.3'
C 1.0 / 22.9'	1258.25	C 1.5 / 23.9'
C 0.5 / 22.5'	1259.22	C 1.0 / 23.3'

Sta	+	H.I.	−	Elev.	Rem.
B.M.	4.78	1265.44		1260.73	
142+0					
142+50					
143+0					
144+0					
T.P.	5.54	1267.51	3.47	1261.97	
145+0					
146+0					
146+50					
147+0					
T.P.	6.51	1271.18	2.84	1264.67	
148+0					

North	℄ Elev	South
Gr. 22.0'	1260.82	Gr. 22.3'
Gr. 22.0'	1261.31	Gr. 22.0'
F 0.5 20.5'	1261.77	F. 0.5 20.5'
F. 0.5 20.7'	1262.47	F. 1.0 20.5'
F. 0.5 20.5'	1263.17	F. 0.5 20.7'
F. 0.5 21.0'	1263.87	F. 1.0 20.1'
F. 0.5 21.0'	1264.25	F. 1.0 20.5'
Gr. 21.9'	1264.67	F. 0.5 20.7'
C. 0.5 22.0'	1265.57	Gr. 21.7'

Sta	+	H.I.	-	Elev.	Rem's
		1271.18			
149+0					
150+0					
T.P.	6.03	1273.80	3.41	1267.77	
B.M.			1.97	1271.80 rec. 1271.83	

North & Elev.		South
F.0.5 / 21.1'	1266.82	F.0.5 / 20.7'
Gr. / 21.3'	1268.77	F.1.0 / 20.5'

FINE GRADE STAKE

Sta	+	H.I.	−	Elev.	Rem's
B.M.	2.46	1072.43		✓1069.97	
0+01				✓1067.29	
0+50				✓1068.18	
1+0			✓	✓1068.65	
1+50			✓	✓1068.90	
2+0			✓	1069.15	
2+50			✓	1069.40	
3+0	C.L.O. on South Side		✓	*1070.00	
3+50			✓	1071.40	
T.P.	6.68	1078.08	1.03	1071.40	
4+0			✓	1077.73	

7/23/31 Cloudy

S. Gold ✓
T. Snyder
D. Parks

Sta	+	H.I.	−	Elev	Rem's
		1078.08			
4+50				✓1073.73	
B.M.	3.73	1078.41	2.90	1075.18 (1075.16 rec)	
5+0				✓ 1074.38	
5+50				✓ 1074.70	
6+0				✓ 1074.85	
6+50				✓ 1075.00	
7+0				✓ 1075.15	
T.P.	4.75	1079.93	3.73	1075.18	
7+50			✓	✓ 1075.30	
8+0			✓	✓ 1075.45	
8+50			✓	✓ 1075.60	

Sta	+	H.I.	−	Elev.	Rem's
		1079.93			
9+0			✓	✓1075.75	
9+50			✓	✓1075.90	
10+0			✓	✓1076.05	
10+50			✓	✓1076.20	
B.M. & T.P.	3.78	1080.70	3.05	1076.92 1076..88	
11+0				✓1076.35	
11+50				✓1076.50	
12+0			✓	✓1076.58	
12+50			✓	✓1076.57	
13+0			✓	✓1076.40	

Sta	+	H.I.	−	Elev.	Rem's
		1080.70			
13+50			✓	✓1076.77	
14+0			✓	✓1076.15	
14+50			✓	✓1075.98	
15+0			✓	✓1075.73	Correct Slope Stakes
T.P.	3.76	1078.99	4.97	1075.73	
15+50			✓	1075.39	
B.M.			4.83	1074.25 1074.16	?
16+0			✓	1074.98 Steel Bar Pk. 1074.96	
B.M.	5.20	1079.45	1074.25		
16+50			✓	1074.45	
17+0			✓	1073.85	
150			✓	1073.17	
T.P.	2.65	1076.90	5.20	1074.25	

Sta	+	H.I.	-	Elev.	Rem's
		1076.90			
18+0			✓	1072.40	
+50			✓	1071.97	
19+0			✓	1072.42	
19+50			✓	1073.56	
20+0			✓	1074.86	
T.P.	3.54	1078.40	2.04	1074.86	
20+25			✓	1075.26	
21+0			✓	1074.46	
21+50			✓	1073.76	
22+0			✓ ✓	1073.06	

Sta	+	H.I.	-	Elev.	Rem's
22+50			✓	1072.36	
23+0			✓	1071.66	
B.M.	4.06	1077.31		1073.25	
			North	South	
23+50			✓1071.65	✓1071.24	
23+68.38 P.C.			1072.03	✓1071.37	
24+0			1072.88	✓1071.81	
+25			✓1073.62	✓1072.31	
+50			✓1074.12	✓1072.81	
+75			✓✓ F.O.S 1074.72	✓1073.31	
25+0			✓ 1075.12	✓1073.81	

Sta	+	H.I.	−	Elev.	Rem's
		1077.31			
			North	South	
25+25			1075.47	1074.29	
25+50			1075.60	1074.75	
T.P.	4.55	1081.30	2.56	1074.75	
25+65.31			1075.66	1075.00	
26+0			1075.66	1075.46 (0.05)	
26+15.31				1075.93	
26+50				1076.40 (0.05 So. Side)	
27+0				1076.96	
27+50				1077.41	
28+0				1077.86	

Sta	+	H.I.	−	Elev.	Rem's
		1081.30			
28+50				1078.20	
T.P.	5.39	1083.69	3.00	1078.30	
29+0				1078.74	
29+50				1079.14	
30+0				1079.53	
30+50				1079.97	
				1080.47 USed	
B.M. & T.P.	4.64	1085.11	3.19	1080.50	
31+0				1080.30	
31+50				1080.68	
32+0				1081.09	
32+50				1081.71	

Sta	+	H.I.	−	Elev.	Rems
		1085.11			
33+0				✓1087.36	
T.P.	5.76	1088.12		1087.36	
+53.60 P.C.			North ✓1087.97	South c.0.5 ✓1087.65	
33+75			✓1083.79	c.0.5 ✓1087.83	
34+0			✓1083.62	c.0.5 ✓1083.01	
34+25			✓ 1083.81	c.0.5 ✓1083.18	
34+50			✓ 1083.85	✓ c.0.5 1083.34	
34+80.98 P.T.			✓ 1083.82	c.0.5 ✓ 1082.50	
35+30.98				✓ 1083.92	
36+0				✓ 1084.76	
T.P.	6.50	1090.76	3.86	1084.76	

Sta	+	H.I.	−	Elev.	Rems
		1090.78			
36+50				✓1084.57	
37+0				✓ 1085.01	
B.M.			5.19	1085.59	
37+50				✓1085.57	
38+0				✓1086.76	
38+50				✓1087.00	
39+0				✓ 1087.65	
39+50				✓1088.20	
T.P.	5.93	1094.13		1088.20	
39+99.0				✓1088.62	
40+50				c.0.5 North ✓ 1088.86	

Sta	+	H.I.	-	Elev.	Remks
		1094.15			
41+0				✓ 1089.15	
41+50				C.I.O.N. ✓ 1089.61	
42+0				✓ 1090.16	
T.P.	6.08	1096.24	3.99	1090.16	
42+50				✓ 1090.71	
43+0				✓ 1091.21	
43+50				✓ 1091.61	
B.M.	3.83	1096.26	3.83	1092.43 1092.41	
44+0				✓ 1091.93	
44+50				✓ 1092.17	
T.P.	5.59	1097.76	4.09	1092.17	
45+0				✓ 1092.39	

Sta	+	H.I.	-	Elev.	Remks
		1097.76			
45+50				✓ 1092.60	
46+0				✓ 1092.92	
46+50				No stake on South Side ✓ 1093.44	
47+0				✓ 1094.06	
T.P.	6.78	1100.84	3.70	1094.06	
47+50				✓ 1094.68	
48+0				✓ 1095.30	
48+50				✓ 1095.92	
49+0				✓ 1096.54	
49+50				✓ 1097.16	
B.M.			4.40	1096.45 Rec'd 1096.44	

Sta	+	H.I.	-	Elev.	Rem's
		1100.84			
50+0			✓	1097.78	
T.P	6.46	1104.24	3.06	1097.78	
50+50			✓	1098.40	
51+0			✓	1099.02	
51+50			✓	1099.64	
52+0			✓	1100.26	
52+50			✓	1100.88	
53+0			✓	1101.50	
+78.65			✓	1101.86	
+50			✓	1102.12	
T.P.	6.79	1108.29		1101.50	
54+0			✓	1102.74	

Sta	+	H.I.	-	Elev.	Rem's
		1106.29			
54+50			✓	1103.36	
55+0			✓	1103.98	
55+50			✓	1104.42	
56+0			✓	1104.50	
56+50			✓	1104.40	
T.P.	5.79	1110.17	3.99	1104.40	
57+0			✓	1104.39	C.05 North
57+50			✓	1104.54	C. 1.0 North
58+0			✓	1104.87	C.1.0 South
58+50			✓	1105.38	

Sta	+	H.I.	-	Elev	Rem
		1110.17			
59+0				1106.05	
59+50			✓	110.79	
				1107.44 rec.	
B.M. & T.P.	7.62	1115.06	2.71	1107.46	
60+0			✓	1107.49	
60+50			✓	1108.15	
61+0			✓	1108.77	
61+50			✓✓	1109.31	
62+0			✓	1109.72	
62+50			✓	1110.01	
63+0			✓	1110.17	
T.P.	4.98	1115.15		1110.17	

Sta	+	H.I.	~~-~~	Elev	Rem's
			North	South C.0.5	
C 3+36.56 P.C.		1115.15	1110.61	1110.09	
5+0			✓ 1110.52	Stak. out 1110.17	
64+0			✓ 1110.85	✓ 1110.22	
5+0			✓ 1110.95	C.0.5. ✓ 1110.32	
65+0			C.1.0 ✓ 1111.05	C.0.5 ✓ 1110.42	
5+0			✓ 1111.15	1110.52	
T.P.	4.11	1115.26	4.00	1111.15	
66+0			✓ 1111.23	✓ 1110.60	
5+0			✓ 1111.18	✓ 1110.55	
67+0			F.0.5 ✓ 1111.14	✓ 1110.51	
1.48 P.T.			✓ 1110.89	C.0.5 1110.57	

Sta	+	H.I.	-	Elev.	Rem's
		1115.24			
68+0			✓	1110.8✓	
B.M. & T.P.	4.79	1116.49	3.54	1111.70 rec. 1111.70	
68+50			✓	1111.27	0.0.15 N 0.0.15 S
69+0			✓	1111.07	
69+50			✓	1111.87	0.0.15 N
70+0			✓	1113.67	C.0.5 N
70+50			✓	1114.47	
T.P.	6.34	1120.81	2.0✓	1114.47	
71+0			✓	1115.27	
71+50			✓	1116.07	
72+0			✓	1116.93	

Sta	+	H.I.	-	Elev.	Rem's
		1120.81			
72+50			✓	1117.9✓	
T.P.	6.95	1124.87	2.89	1117.9✓	
73+0			✓	1118.97	
73+50			✓	1120.0✓	
74+0			✓	1121.07	
74+50			✓	1121.47	
B.M.			1.9✓	1122.95 rec. 1122.9✓	
75+0			✓	1121.20	
T.P.	4.88	1126.08	3.67	1121.20	
75+50			✓	1121.14	F.0.5 South
76+0			✓	1121.5✓	C.1.0 South
76+50			✓	1122.1✓	

Sta	+	H.I.	-	Elev	Rem.
		1176.08			
77+0			✓	1172.7✓	
77+50			✓	1173.3✓	
T.P.	5.25	1178.57	4.76	1173.3✓	
78+0			✓	1173.9✓	
78+50			✓	1174.57	
79+0			✓	1175.53	-
79+50			✓	1177.1✓	
T.P.	6.95	1134.09	1.45	1177.1✓	
80+0			✓	1179.0✓	
B.M.			4.06	1130.00 rec. 1130.03	
80+50			✓	1130.9✓	C.0.5 N.
81+0			✓	1137.8✓	
T.P.	9.79	1142.11		1137.84	

Sta	+	H.I.	-	Elev.	
		1147.11			
81+73.95			✓	1133.66	
81+50			✓	1134.4✓	
82+0			✓	1135.4✓	
82+50			✓	1136.1✓	
83+0			✓	1136.8✓	
83+50			✓	1137.5✓	C.0.5 N.
84+0			✓	1138.2✓	
84+50			✓	1138.9✓	
85+0			✓	1139.6✓	
B.M.		1147.11	1.03	1141 or rec. 1141.08	✓

Sta	+	H.I.	−	Elev	Rem's
		1147.11			
85+50			✓	1140.37	
T.P.	5.95	1146.27	1.79	1140.32	
86+0			✓	1141.07	
86+50			✓	1141.77	
87+0			✓	1142.47	
87+50			✓	1143.41	
88+0			✓	1144.98	C.1.0 S. C.0.5 N.
T.P.	8.50	1153.98	.79	1145.48	
88+50			✓	1146.84	C.0.5 S.
89+0			✓	1148.70	C.1.0 S. C.1.0 N.
89+50			✓	1150.74	C.1.0 N. C.0.5 S.

Sta	+	H.I.	−	Elev.	Rem's
		1158.98			
90+0			✓	1153.14	C.0.5 S. C.0.5 N.
T.P.	8.89	1162.53	0.34	1153.64	
90+50			✓	1155.90	
B.M.			2.45	1160.10 Rec— 1160.08	
91+0			✓	1159.07	
91+50			✓	1162.37	
T.P.	12.01	1174.33		1162.37	
92+0			✓	1165.67	
92+50			✓	1168.97	
93+0			✓	1171.27	C.0.5 N.
T.P.	9.66	1183.89	.10	1174.23	
93+50			✓	1175.30	C.1.0 N. C.1.0 S.
94+0			✓	1177.97	C.1.0 S. C.0.5 N.

Sta	+	H.I.	-	Elev	Rem's
		1183.89			
94+50			✓	1180.10	C.0.5.S
95+0			✓ ✓	1181.8✓	C.0.5.S C.0.5.N
95+50			✓ ✓	1183.3✓	C.0.5.N
T.P.	7.58	1190.94	0.53	1183.36	
96+0			✓ ✓	1184.61	
96+50			✓ ✓	1185.47	
97+0			✓ ✓	1186.1✓	
97+50			✓	1186.77	✓
T.P.	5.78	1192.6✓	4.17	1186.83	
98+0			✓	1187.42	
B.M.			4.13	1188.49 1188.49	✓
98+50			✓	1188.07	C.0.5.S

Sta	+	H.I	-	Elev.	Rem's
		1192.6✓			
99+0			✓	1188.68	
99+50			✓	1189.3✓	
100+0			✓	1189.7✓	
T.P.	5.73	1195.45	2.90	1189.7✓	
100+50			✓	1190.3✓	
101+0			✓	1190.7✓	
101+50			✓	1191.33	
102+0			✓	1192.17	
102+50			✓	1193.1✓	C.0.5 S.
T.P.	6.78	1199.90	2.33	1193.1✓	
103+0			✓	1194.07	

Sta	+	H.I.	-	Elev	Rem's
		1199.90			
103+50			✓	1195.07✓	
104+0			✓	1195.97	
104+50			✓	1196.9✓	
105+0			✓	1197.67	
T.P.	7.72	1205.59	2.03	1197.87	
105+50			✓	1198.98	
106+0			✓	1200.4✓	0.0.5S.
106+50			✓	1201.0✓	0.1.0 S.
107+0			✓	1203.6✓	
107+50			✓	1205.2✓	
T.P.	8.22	1213.44	0.37	1205.22	

Sta	+	H.I.	-	Elev	Rem's
		1213.44			
108+0			✓	1206.8✓	C.1.0 S.
108+50			✓	1208.4✓	C.0.5.S
109+0			✓	1210.0✓	
+35				1210.7✓	
109+50			✓	1211.23	C.1.0 S.
+35				1211.55	
110+0			✓	1211.67	C.0.5 N.
+35				1211.60	
110+79.56			✓	1211.55	C.0.5 S. 0.0.5 N
T.P.	4.06	1215.73		1211.67	
110+50			✓	1211.33	
+35				1210.87	
111+0			✓	1210.22	
111+50			✓	1208.34	
T.P.	0.86	1209.17	7.42	1208.31	

Sta	+	H.I.	-	Elev.	Rem's
		1209.17			
112+0			✓	1205.70	
B.M.			3.44	1205.71	1205 Gl rec. B.M. has been Disturbed
112+50			✓	1202.68	C.0.5 S.
113+0			✓	1199.66	C.0.5 S
T.P.	1.61	1201.77	9.01	1200.16	
113+50			✓	1196.80	C.0.5 S. C.0.3 N.
113+75			✓	1195.73	
114+0			✓	1194.95	C.0.5 S.
114+25			✓	1194.46	C.0.5 S
T.P.	5.49	1199.95		1194.46	
114+31			✓	1194.41	
114+50			✓	1194.27	

Sta	+	H.I.	-	Elev	Rem's
		1199.95			
114+75			✓	1194.37	
115+0			✓	1194.79	
115+15.5			✓	1195.26	
115+25			✓	1195.54	
115+50			✓	1196.62	
115+75			✓	1198.04	
116+0			✓	1199.79	
T.P.	9.81	1209.60	0.16	1199.79	
116+25			✓	1201.87	
116+50			✓	1204.12	

Sta	+	H.I.	−	Elev.	Rem's
		1209.60			
117+0			✓	1208.62	
T.P.	10.85	1219.47	.98	1208.62	
117+50			✓	1213.12	0.1.0 S.
118+0			✓	1217.62	C.0.5 S.
T.P.	11.83	1229.45	1.85	1217.62	
118+50			✓	1222.12	C.0.5 N. C.0.5 S.
119+0			✓	1226.62	
T.P.	10.45	1239.57	0.33	1229.12	
119+50			✓	1230.72	
120+0			✓	1234.02	
120+50			✓	1236.92	
T.P.	12.63	1251.07	1.13	1238.44	
121+0			✓	1239.82	

Sta	+	H.I.	−	Elev.	Rem's
		1251.07			
121+50			✓	1242.72	
122+0			✓	1245.40	
122+50			✓	1247.62	
123+0			✓	1249.62	
T.P.	7.10	1256.53	1.64	1249.43	
123+50			✓	1251.41	
B.M.			3.90	1252.62	
124+0	4.77	1257.54	✓	1252.77	
T.P.				1257.77	
124+50			✓	1253.71	C.0.5 N
125+0			✓	1254.22	
125+50			✓	1254.31	

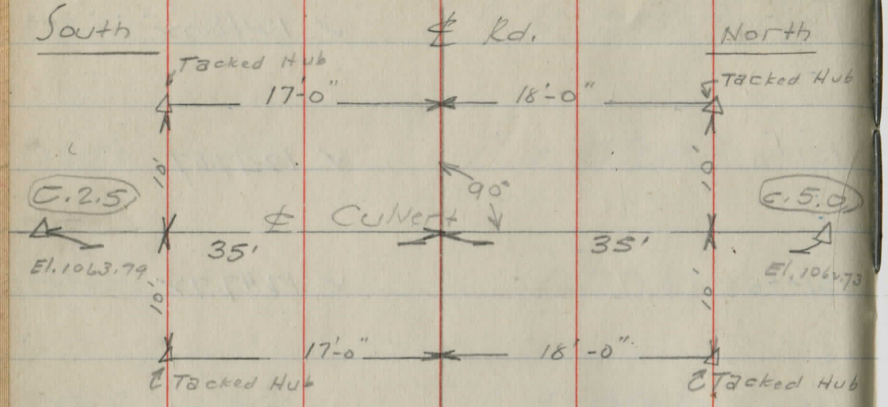
Sta	+	H.I.	−	Elev.	Rem'k
		1257.54			
126+0			✓	1253.97	
126+50			✓	1253.42	
127+0			✓	1252.87	
127+50			✓	1252.32	
128+0			✓	1251.68	
T.P.	7.00	1253.68	5.86	1247.68	
128+50			✓	1250.87	
129+0			✓	1249.97	
B.M.			4.12	1249.56	
129+57			✓	1248.97	
129+50				1249.07	
130+0			✓	1248.36	

Sta	+	H.I	−	Elev.	Rem'k
		1253.68			
130+50			✓	1248.02	
131+0			✓	1247.87	
131+50			✓	1247.72	
132+0			✓	1247.57	
T.P.	4.58	1252.15	6.11	1247.57	
132+50			✓	1247.47	
133+0			✓	1247.45	
133+50			✓	1247.53	
134+0				1247.70	
134+50			✓	1247.96	

S Gold Jr.
A.J. Rhodes

Thompson-Leroy Rd. April 23, 1931
Cold. Windy

Sta 2+10.0



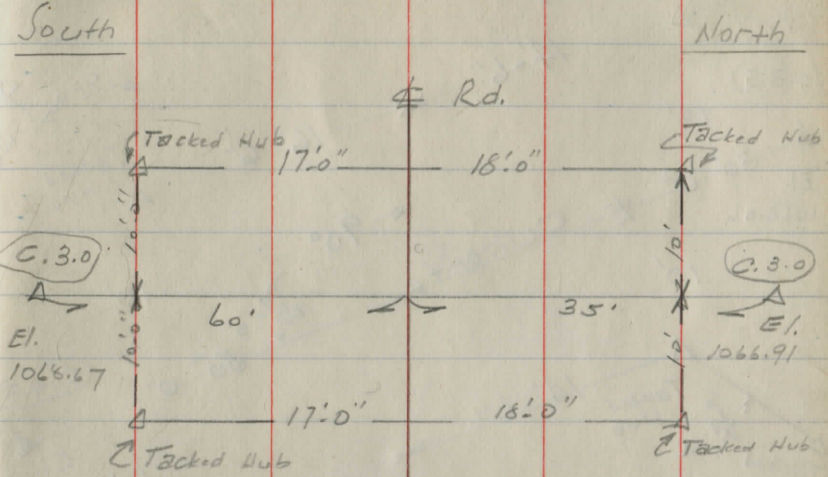
4' x 3' x 33' Box culvert

Tacked Hubs set on 1' offset

South F.L. Elev. 1063.50

North " " " 1063.00

Sta 18+63



4' x 3' x 27' Box culvert

Tacked Hubs set on 4' offset

South F.L. El. 1067.60

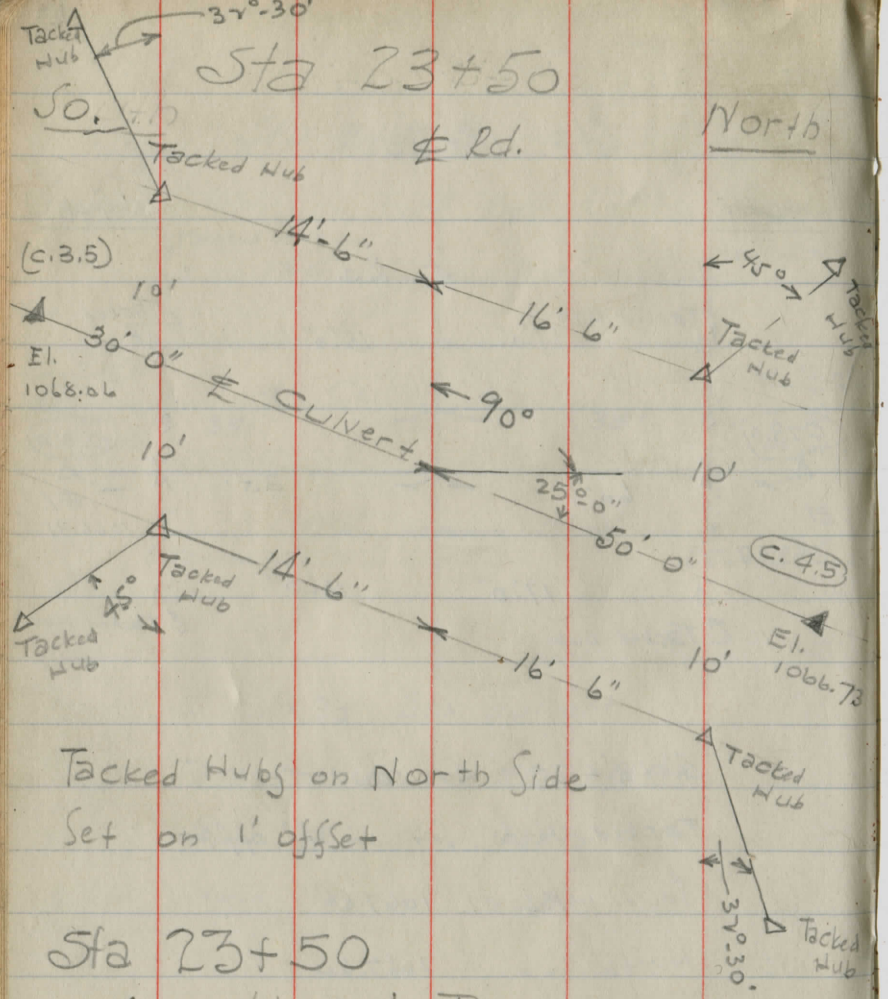
North " " " 1067.30

Sta 23+50

So.

℄ Rd.

North



Tacked Hubs on North Side
Set on 1' offset

Sta 23+50
4' x 2½' x 30' Box Culvert
25° Skew

Sta 35+84

sunny mild ±65° Thompson Rd Sec "C"
Nov. 6 57
Patterson Temple

	Elev +	Culvt HI	Sta −	57+68 Elev
BM # 11	3.28	1114.98		1111.70
TP	2.72	1111.41	6.29	1108.69
BM # 10			5.16	1106.25 New Elev
TP	5.28	1114.58	2.11	1109.30
BM # 11			2.84	1111.74
BM # 10	2.98	1109.23		1106.25
57+68				
57+18				
57+68				9'6"x26"x20' Conc. Slab Culvt.
57+18				
56+68				

℄

1102.23
5.00

1098.63 1099.13 1103.93 1103.83 1099.33
5.30

℄ Stream 110' FL. ℄ FL ℄ Stream 120' 200'
10.60 10.10 3.4 9.90 9.20 9.10
X X X X X X

1103.37
5.86

1103.13
6.10

℄

Sta 84+80

Sta 133+45

Sta	+	H.I.	-	Elev.	Rem's
		1252.15			
135+0			✓	1248.32	
135+50			✓	1248.72	
136+0			✓	1249.12	
136+50			✓	1249.60	
T.I.					
137+0			✓	1250.22	
T.P. ✓	10.11	1260.33	1.93	1250.22	
137+50			✓	1251.00	
138+0			✓	1251.92	
138+50			✓	1252.98	
139+0			✓	1254.17	

Sta	+	H.I.	-	Elev	Rem's
		1260.33			
139+50			✓	1255.48	
140+0			✓	1256.92	
140+57 used ~~140+50~~			✓	1258.39 used ~~1258.25~~	
141+0			✓	1259.22	
T.P.	7.66	1264.58	3.41	1256.92	
141+50			✓	1260.02	
B.M.			3.86	1260.73 r.c. 1260.72	
142+0			✓	1260.82	
142+50			✓	1261.31	
143+0			✓	1261.77	
143+50			✓	1262.12	
T.P.	4.69	1266.81	2.46	1262.12	
144+0			✓	1262.47	

Sta	+	H.I.	-	Elev	Remrk
		1266.81			
144+50			✓	1262.87	
145+0			✓	1263.17	
145+50			✓	1263.57	
146+0			✓	1263.87	
146+50			✓	1264.25	
T.P.	5.77	1270.02	2.56	1264.25	
147+0			✓	1264.67	
147+50			✓	1265.17	
148+0			✓	1265.57	
148+50			✓	1266.11	

Sta	+	H.I.	-	Elev	Remrk
		1270.02			
149+0			✓	1266.87	
149+50			✓	1267.71	
T.P.	5.87	1273.53	2.31	1267.71	
150+0			✓	1268.47	
150+50			✓	1270.01	
151+0				1271.42	
B.M.			1.72	1270.80 rec - 1271.81	

12-5-41 Graber Fomeroy

Levels N of culv't Sta. (133+45?)

BM II 21	1.26	1261.99		1260.73 ← pg. 3
T.P.	1.05	1252.87	10.17	1251.82
F.L.			9.15	1243.72
N. Hdwl			5.10	1247.77
1			stk 6.04	1246.83
			ch 9.26	1243.61
2			stk 6.29	1246.58
			ch 9.75	1243.12
T.P.	2.61	1249.19	6.29	1246.58
3			s 3.10	1246.09
			c 6.3	1242.9
4			s 3.12	1246.07
			c 6.7	1242.5
5			s 3.56	1245.63
			c 7.4	1241.8
6			s 5.43	1243.76
			c 8.7	1240.5
6+70			s 5.95	1243.24
			c 9.9	1239.3

74

4'x2' Conc Box at 133+45

		1249.19		
7+0			s 6.13	1243.06
			c 10.55	1238.64
T.P.	1.11	1244.19	6.11	1243.08
7+0			c 5.6	1238.6
8+0			s 2.34	1241.85
			c 6.8	1237.4
9+0			s 2.86	1241.33
			c 7.5	1236.7
10+0			s 4.53	1239.66
			c 8.2	1236.0
11+0			s 4.93	1239.26
			c 9.6	1234.6

3-10-56 Patterson Canfield

Thompson Road (± ½ mi West of Rt. 528)

Levels N & W of Culvt. Sta 133+45

	+	H.I.	-	Elev
BM #A	4.01	1252.03 ~~1004.01~~	3.40	1248.02 ~~1000.00~~
North Road Ditch running West				
T.P. Elev. Front	5.47	1254.10 ~~1006.08~~	1.23	1248.63 ~~1000.61~~
T.P. Elev. Back	3.89	1256.76 ~~1008.74~~	1.88	1252.87 ~~1004.85~~
T.P.	5.10	1259.98 ~~1011.96~~	4.15	1254.88 ~~1006.86~~
T.P	2.84	1258.67 ~~1010.65~~	3.79	1255.83 ~~1007.81~~

75

N S

X Cut in SE 7 S. Culvt Hdwl Sta 133+~~28~~ 45

42.4 42.8 43.3 43.7 O.L. Drain N Ditch 44.45 N-Culv Hdwl. ℄ S Ditch

9.6/400 9.2/300 8.7/200 8.5/150 8.15/100' 7.7/75' 7.5/50' 7.58 4.26 4.9 7.66

W 6.5/O.L. Drain 6.8/225' 7.0/150' 7.15/75' E

F. Paine Front

Ditch 4.88 1.57 52.5 1.62 52.5

52.33

1.77 Sill + 5.8 = Elev. 1246.53

4.37? + 5.86? = 46.53

~~2.37~~ Sill + ~~6.86~~ = Elev. ~~1247.53~~

Back F. Paine

℄ Road 4.21/100'W 4.87/Sta 129+30 5.7/100' E ~~8~~7.0/250' E

M. Feko Front

3.0 + 7.1 = Elev. 1249.88

2.4 2.3

Sta 124+00

5.06 5.44 ℄ Drive Culvt. plugged with Trash

	+	H.I	-	Elev.
		1258.67		1255.83
	2.84	~~1018.65~~	3.79	~~1007.81~~
T.P.	3.10	1257.98	2.78	1254.88
		~~1009.96~~		~~1006.86~~
T.P.	2.14	1257.34	8.50	1255.20
		~~1003.32~~		~~1007.18~~
T.P.	3.0	1251.84	3.99	1248.84
		~~1003.82~~		~~1000.82~~
B.M				1247.85
				~~999.83~~

Drain
OL
6.7

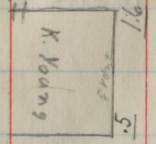
S
Pitch
6.8

E
5.5

N
Ditch
6.7

1.77 + 5.98 =

Elev. 1250.92



June 26, 1957
H. Patterson
D. Canfield
T. Adams

Thompson Rd. Profile

Warm
Clear

	+	HI	−	Elev
B.M.	10.96	1262.83		1251.87
18+0			10.75	
+50			9.33	
17+0			.16	
TP	11.30	1272.49	1.64	1261.19
16+0			.32	
TP	9.99	1282.16	.32	1272.17
15+0			5.11	
14+0			8.66	
13+0			11.59	
TP	0.01	1270.42	11.75	1270.41
12+0			1.53	
11+0			3.00	
10+0			4.03	

	+	HI	−	Elev	
		1270.42			
9+0			4.97		
Vert. Spk. W. Root Wild Cherry 8' Left &					18+08
8+0			5.71		
7+0			6.22		
6+0			6.35		
5+0			5.60		
4+0			4.32		
3+0			2.75		
TP	11.70	1279.37	2.75	1267.67	
2+0			7.94		
+50			4.38		
1+0			2.40		
0+0			4.04		
T.P.	0.10	1279.32	.15	1279.22	

	+	HI	-	Elev
		1279.32		
USGS BM			3.20	1276.12
BM	2.00	1253.87		1251.87
18+50			7.03	
19+00			12.0	
TP	1.15	1243.86	11.16	1242.71
TP	.58	1232.51	11.93	1231.93
20+00			2.12	
TP & 21+00	1.09	1221.77	11.83	1220.68
22+00			8.69	
TP & 23+00	.73	1210.52	11.98	1209.79
24+00			5.76	
TP & 25+00	.58	1199.54	11.56	1198.96

	+	HI	-	Elev
		1199.54		
26+00			7.17	
TP	.78	1193.18	7.14	1192.40
27+00			5.96	
TP & 28+00	1.09	1183.74	10.53	1182.65
29+00			5.41	
TP & 30+00	.31	1174.10	9.95	1173.79
31+00			4.24	
TP & 32+00	.74	1166.83	8.01	1166.09
33+00			4.56	
34+00			9.94	
35+00			14.10	

	+	HI 1166.83	−	Elev	
TP	1.24	1156.62	11.45	1155.38	
36+0			5.55		
+18.5			5.20		
B.M.			5.46	1151.16	X SW ⊥ N Hdwl in N.W. Quad ⊥ ⊥ Under Rd (CK #42)

PLEASE RETURN TO
GEAUGA COUNTY ENGINEER
COURT HOUSE
CHARDON, O.
PHONE 250-X

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 14 feet wide, side slopes 1½ to 1.

For Single Track Embankment.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

MADE IN GERMANY.

R.